

# Method of Matrices Operations in H2 Control for Calcium Ion Channel on the Biological Membrane as a Closed Circuit.

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あらし

I have proposed an h2 control principle for bio chemical noise filtering function of the calcium in channel on the excitable cellular membrane. The Calcium channel is composed of four identical subunits. Each of which contains a helical segment which contains a lot of electrical charge that acts as a membrane voltage sensor. The opening and closing of the channel pore are facilitated by the activating positionings of the voltage sensor. The temporal changes in the system were described by ten differential equations under the condition that minimizes the 2 norm of the transfer function of the system from the noise input the out put. The computed temporal changes in the open and closed states are significantly influenced by the changes in the amounts of the control inputs. The present methods, when extended will be available for evaluating the filtering function of the bio membranes.

和文キーワード Bio membrane, calcium in, Channel, Subunits, Voltage sensor, H2 control, Noise, 2 norm.

## 閉回路としてのカルシウムイオンチャンネルのH2制御

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Abstract

カルシウムイオンを選択的に通過させるカルシウムイオンチャンネルの機能特性を雑音フィルターの視点からH2制御を用いて解析する方法を提唱した。カルシウムイオンチャンネルは4個の相同性の高いサブユニットから構成されている。また膜電位感受性を有するタンパク分子がそれぞれのサブユニットに付属し、その空間内の位置が変化することでチャンネル開閉が加速される。本研究では10個のチャンネル構造を10個の状態方程式で表示し、雑音が出力されるまでの系の伝達関数の2ノルムを最少にする場合のチャンネルの状態の過渡的状況を数値計算で決定した。制御入力の変化によって開状態、閉状態のチャンネルの時間経過を大きく影響された。本研究を発展させることで生体膜チャンネルの生化学的雑音低減効果を評価できる可能性を示唆した。

英文 key words 生体膜. カルシウムイオン. チャンネル. H2制御. 雑音. 伝達関数 2ノルム

**1. Introduction.**

Calcium channel ( Fig 1 ) on the excitable membrane filters only Calcium ion though there are a lot of agonist and antagonist that compete the channel with Calcium ion. Hence, the mechanism can be described by the H2 control principle. The dynamical action of the Calcium channel is characterized by four identical subunits (Fig 2) that act concertedly. The channel opening and closing are strongly influenced by a particular segment named S4 ( Fig 3 ) which has a high voltage sensing property in each subunits. S4 contains a lot of charges on its surface. When it takes the activating position in the subunit, the transitions among the open states are facilitated. By the spatial consideration of the activating positionings of the voltage sensor, we have ten conformations of one Calcium channel. (Fig 4-a and Fig 4-b).

In the present work, we present a detailed matrix expansion for computing the H2 controlled temporal change of the amounts of the Calcium channel states.

**2. Mathematical method.**

The state equations for these ten conformation states are given by linear combination of weighted control inputs.

Fig 1

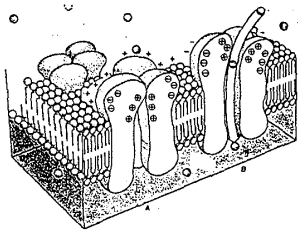


Fig 2



Fig 3

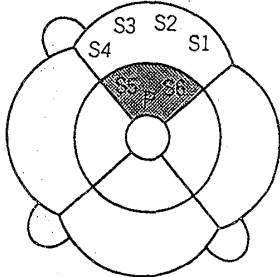
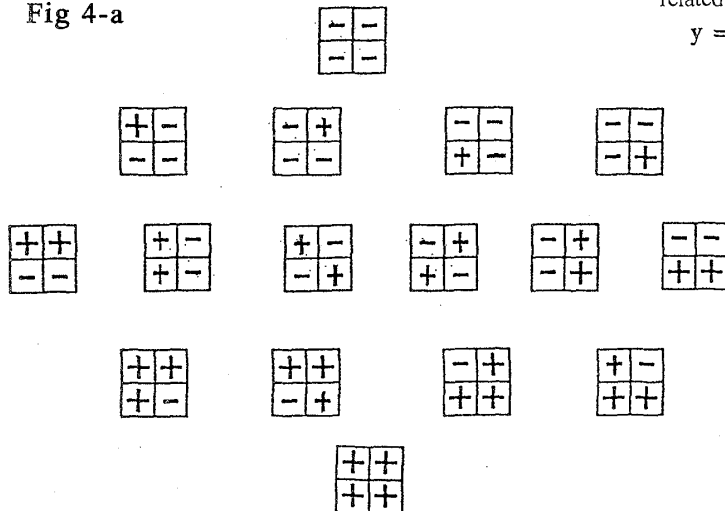


Fig 4-a



$$\begin{aligned} \partial C_0 / \partial t &= k-c C_1 + k-L / f_4 O_0 - ( 4 k c + k_L f_4 ) C_0 \\ &\quad + p_9' u_3 + p_1' u_1 \quad \text{-----(1)} \\ \partial C_1 / \partial t &= 4 k c C_0 + 2 k-c C_2 + k-L / f_3 O_1 - ( k-c + 3 k c + \\ &\quad k_L f_3 ) C_1 + p_1 u_1 + p_{10}' u_3 + p_2' u_1 \quad \text{-----(2)} \\ \partial C_2 / \partial t &= 3 k c C_1 + 3 k-c C_3 + k-L / f_2 O_2 - ( 2 k-c + 2 k \\ &\quad + k_L f_2 ) C_2 + p_2 u_1 + p_{11}' u_3 + p_3' u_1 \quad \text{-----(3)} \\ \partial C_3 / \partial t &= 2 k c C_2 + 4 k-c C_4 + k-L / f O_3 - ( 3 k-c + k c + k_L f ) \\ &\quad C_3 + p_3 u_1 + p_{12}' u_3 + p_4' u_1 \quad \text{-----(4)} \\ \partial C_4 / \partial t &= k c C_3 + k-L O_4 - ( 4 k-c + k_L ) C_4 \\ &\quad + p_4 u_1 + p_{13}' u_3 \quad \text{-----(5)} \\ \partial O_0 / \partial t &= f_4 k_L C_0 + k-c f O_1 - ( k-L / f_4 + 4 k c / f ) O_0 \\ &\quad + p_9 u_3 + p_5' u_2 \quad \text{-----(6)} \\ \partial O_1 / \partial t &= 4 k c / f O_0 + k_L f_3 C_1 + 2 k-c f_2 O_2 \\ &\quad - ( k-c f + k-L / f_3 + 3 k c / f_2 ) O_1 + p_{10} u_3 + p_6' u_2 \quad \text{---(7)} \\ \partial O_2 / \partial t &= 3 k c / f_2 O_1 + k_L f_2 C_2 + 3 k-c f_3 O_3 \\ &\quad - ( 2 f_2 k-c + k-L / f_2 + 2 k c / f_3 ) O_2 + p_{11} u_3 + p_7' u_2 \quad \text{---(8)} \\ \partial O_3 / \partial t &= 2 k c / f_3 O_2 + k_L f C_3 + 4 k-c f_4 O_4 - ( 3 k-c f_3 \\ &\quad + k-L / f + k c / f_4 ) O_3 + p_7 u_2 + p_{12} u_3 + p_8' u_2 \quad \text{----(9)} \\ \partial O_4 / \partial t &= k c / f_4 O_3 + k_L C_4 - ( 4 k-c f_4 + k-L ) O_4 \\ &\quad + p_8 u_2 + p_{13} u_3 \quad \text{----(10)} \end{aligned}$$

The vector form

$$\partial x'(t) / \partial t = A x + B_1 w + B_2 u$$

Vector form of the equation for the estimator Z

$$Z = C_1 x + D_{12} u$$

Vector form of the equation for the observer output y

$$y = C_2 x + D_{21} w$$

The vector for of the optimized control u^ is given by the product of B2, X and x^

$$u^ = - B_2 T X x^$$

where x^ is the state vector of the observers and T denotes transpose.

$x^T = [ x_{10}, x_{11}, x_{12}, x_{13}, x_{14}, x_{15}, x_{16}, x_{17}, x_{18} ]^T$  which correspond to state variables. X is the solution of related algebraic Riccati equation.

$$A T X + X A - X B_2 B_2 T X + C_1 T C_1 = 0$$

The vector equation of observer x^ is given by

$$\partial x^ / \partial t = A x^ + B_2 u + Y C_2 T ( y - C_2 x^ )$$

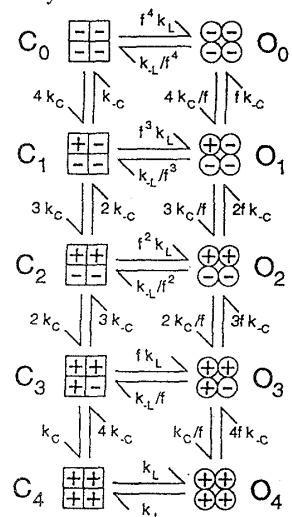
where Y is the solution of adjoint algebraic Riccati equation

$$A Y + Y A T - Y C_2 T C_2 Y + B_1 B_1 T = 0$$

To close the feed back loop of the system, y can be related to state variable x by

$$y = x d - C_2 x$$

Fig 4-b



$$A = \begin{bmatrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & a_{16} & a_{17} & a_{18} & a_{19} \\ a_{21} & 0 & a_{23} & 0 & 0 & 0 & 0 & 0 & a_{29} \\ 0 & a_{32} & 0 & a_{34} & 0 & 0 & 0 & a_{38} & 0 \\ 0 & 0 & a_{43} & 0 & a_{45} & 0 & a_{47} & 0 & 0 \\ 0 & 0 & 0 & a_{54} & 0 & a_{56} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & a_{65} & 0 & a_{67} & 0 & 0 \\ 0 & 0 & 0 & a_{74} & 0 & a_{76} & 0 & a_{78} & 0 \\ 0 & 0 & a_{83} & 0 & 0 & 0 & a_{87} & 0 & a_{89} \\ a_{91} & a_{92} & a_{93} & a_{94} & a_{95} & a_{96} & a_{97} & a_{98} & a_{99} \end{bmatrix};$$

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$$\begin{bmatrix} 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$B_2^T = \begin{bmatrix} b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix}$$

**Matrix form of the Riccati solution X is**

X =

$$\begin{bmatrix} X_{11} & X_{12} & X_{13} & X_{14} & X_{15} & X_{16} & X_{17} & X_{18} & X_{19} \\ X_{12} & X_{22} & X_{23} & X_{24} & X_{25} & X_{26} & X_{27} & X_{28} & X_{29} \\ X_{13} & X_{23} & X_{33} & X_{34} & X_{35} & X_{36} & X_{37} & X_{38} & X_{39} \\ X_{14} & X_{24} & X_{34} & X_{44} & X_{45} & X_{46} & X_{47} & X_{48} & X_{49} \\ X_{15} & X_{25} & X_{35} & X_{45} & X_{55} & X_{56} & X_{57} & X_{58} & X_{59} \\ X_{16} & X_{26} & X_{36} & X_{46} & X_{56} & X_{66} & X_{67} & X_{68} & X_{69} \\ X_{17} & X_{27} & X_{37} & X_{47} & X_{57} & X_{67} & X_{77} & X_{78} & X_{79} \\ X_{18} & X_{28} & X_{38} & X_{48} & X_{58} & X_{68} & X_{78} & X_{88} & X_{89} \\ X_{19} & X_{29} & X_{39} & X_{49} & X_{59} & X_{69} & X_{79} & X_{89} & X_{99} \end{bmatrix}$$

**The control input is**

$$u^{\wedge} = -B_2^T X x^{\wedge}$$

$B_2^T X =$

$$\begin{bmatrix} X_{11} & X_{12} & X_{13} & X_{14} & X_{15} & X_{16} & X_{17} & X_{18} & X_{19} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix}$$

=

$$b_{11} X_{16} + b_{13} X_{17} + b_{15} X_{18} + b_{17} X_{19} \quad : \quad Xb_{11}$$

$$b_1 X_{11} + b_3 X_{12} + b_5 X_{13} + b_7 X_{14} + b_9 X_{15} \quad : \quad Xb_{21}$$

$$b_2 X_{11} + b_4 X_{12} + b_6 X_{13} + b_8 X_{14} + b_{10} X_{15} + b_{12} X_{16} + b_{14} X_{17} + b_{16} X_{18} + b_{18} X_{19} \quad : \quad Xb_{31}$$

$$\begin{bmatrix} X_{12} & X_{22} & X_{23} & X_{24} & X_{25} & X_{26} & X_{27} & X_{28} & X_{29} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix}$$

$$b_{11} X_{36} + b_{13} X_{37} + b_{15} X_{38} + b_{17} X_{39} \quad : \quad Xb_{13}$$

$$b_1 X_{13} + b_3 X_{23} + b_5 X_{33} + b_7 X_{34} + b_9 X_{35} \quad : \quad Xb_{23}$$

$$b_2 X_{13} + b_4 X_{23} + b_6 X_{33} + b_8 X_{34} + b_{10} X_{35} + b_{12} X_{36} + b_{14} X_{37} + b_{16} X_{38} + b_{18} X_{39} \quad : \quad Xb_{33}$$

$$\begin{bmatrix} X_{14} & X_{24} & X_{34} & X_{44} & X_{45} & X_{46} & X_{47} & X_{48} & X_{49} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix} =$$

$$b_{11} X_{46} + b_{13} X_{47} + b_{15} X_{48} + b_{17} X_{49} \quad : \quad Xb_{14}$$

$$b_1 X_{14} + b_3 X_{24} + b_5 X_{34} + b_7 X_{44} + b_9 X_{45} \quad : \quad Xb_{24}$$

$$b_2 X_{14} + b_4 X_{24} + b_6 X_{34} + b_8 X_{44} + b_{10} X_{45} + b_{12} X_{46} + b_{14} X_{47} + b_{16} X_{48} + b_{18} X_{49} \quad : \quad Xb_{34}$$

$$\begin{bmatrix} X_{15} & X_{25} & X_{35} & X_{45} & X_{55} & X_{56} & X_{57} & X_{58} & X_{59} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix} =$$

$$b_{11} X_{56} + b_{13} X_{57} + b_{15} X_{58} + b_{17} X_{59} \quad : \quad Xb_{15}$$

$$b_1 X_{15} + b_3 X_{25} + b_5 X_{35} + b_7 X_{45} + b_9 X_{55} \quad : \quad Xb_{25}$$

$$b_2 X_{15} + b_4 X_{25} + b_6 X_{35} + b_8 X_{45} + b_{10} X_{55} + b_{12} X_{56} + b_{14} X_{57} + b_{16} X_{58} + b_{18} X_{59} \quad : \quad Xb_{35}$$

$$\begin{bmatrix} X_{16} & X_{26} & X_{36} & X_{46} & X_{56} & X_{66} & X_{67} & X_{68} & X_{69} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix} =$$

$$b_{11} X_{66} + b_{13} X_{67} + b_{15} X_{68} + b_{17} X_{69} \quad : \quad Xb_{16}$$

$$b_1 X_{16} + b_3 X_{26} + b_5 X_{36} + b_7 X_{46} + b_9 X_{56} \quad : \quad Xb_{26}$$

$$b_2 X_{16} + b_4 X_{26} + b_6 X_{36} + b_8 X_{46} + b_{10} X_{56} + b_{12} X_{66} + b_{14} X_{67} + b_{16} X_{68} + b_{18} X_{69} \quad : \quad Xb_{36}$$

$$\begin{bmatrix} X_{17} & X_{27} & X_{37} & X_{47} & X_{57} & X_{67} & X_{77} & X_{78} & X_{79} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix} =$$

$$b_{11} X_{67} + b_{13} X_{77} + b_{15} X_{78} + b_{17} X_{79} \quad : \quad Xb_{17}$$

$$b_1 X_{17} + b_3 X_{27} + b_5 X_{37} + b_7 X_{47} + b_9 X_{57} \quad : \quad Xb_{27}$$

$$b_2 X_{17} + b_4 X_{27} + b_6 X_{37} + b_8 X_{47} + b_{10} X_{57} + b_{12} X_{67} + b_{14} X_{77} + b_{16} X_{78} + b_{18} X_{79} \quad : \quad Xb_{37}$$

$$\begin{bmatrix}
 X_{19} & X_{29} & X_{39} & X_{49} & X_{59} & X_{69} & X_{79} & X_{89} & X_{99} \\
 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\
 b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\
 b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18}
 \end{bmatrix}$$

=

$$\begin{aligned}
 & b_{11} X_{69} + b_{13} X_{79} + b_{15} X_{89} + b_{17} X_{99} & : X_{b19} \\
 & b_1 X_{19} + b_3 X_{29} + b_5 X_{39} + b_7 X_{49} + b_9 X_{59} & : X_{b29} \\
 & b_2 X_{19} + b_4 X_{29} + b_6 X_{39} + b_8 X_{49} + b_{10} X_{59} \\
 & + b_{12} X_{69} + b_{14} X_{79} + b_{16} X_{89} + b_{18} X_{99} & : X_{b39}
 \end{aligned}$$

Them,we have

$$u = - B_2^T X x^{\wedge}$$

=

$$\begin{bmatrix}
 X_{b11} & X_{b12} & X_{b13} & X_{b14} & X_{b15} & X_{b16} & X_{b17} & X_{b18} & X_{b19} \\
 X_{b21} & X_{b22} & X_{b23} & X_{b24} & X_{b25} & X_{b26} & X_{b27} & X_{b28} & X_{b29} \\
 X_{b31} & X_{b32} & X_{b33} & X_{b34} & X_{b35} & X_{b36} & X_{b37} & X_{b38} & X_{b39}
 \end{bmatrix}$$

$$[ x_{10} x_{11} x_{12} x_{13} x_{14} x_{15} x_{16} x_{17} x_{18} ]^T$$

=

$$\begin{aligned}
 & - [ X_{b11} X_{10} + X_{b12} X_{11} + X_{b13} X_{12} + X_{b14} X_{13} + X_{b15} X_{14} + X_{b16} X_{15} + X_{b17} X_{16} + X_{b18} X_{17} + X_{b19} X_{18} \\
 & X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18} \\
 & X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18} ]
 \end{aligned}$$

$$B_2 = \begin{bmatrix}
 0 & b_1 & b_2 \\
 0 & b_3 & b_4 \\
 0 & b_5 & b_6 \\
 0 & b_7 & b_8 \\
 0 & b_9 & b_{10} \\
 b_{11} & 0 & b_{12} \\
 b_{13} & 0 & b_{14} \\
 b_{15} & 0 & b_{16} \\
 b_{17} & 0 & b_{18}
 \end{bmatrix}$$

B2 u =

$$\begin{aligned}
 & b_1 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\
 & + b_2 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\
 & b_3 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\
 & + b_4 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\
 & b_5 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\
 & + b_6 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\
 & b_7 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\
 & + b_8 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\
 & b_9 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\
 & + b_{10} (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\
 & b_{11} (X_{b11} X_{10} + X_{b12} X_{11} + X_{b13} X_{12} + X_{b14} X_{13} + X_{b15} X_{14} + X_{b16} X_{15} + X_{b17} X_{16} + X_{b18} X_{17} + X_{b19} X_{18}) \\
 & + b_{12} (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18})
 \end{aligned}$$

$$b13(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13 + Xb15 X14 + Xb16 X15 + Xb17 X16 + Xb18 X17 + Xb19 X18 + b14 (Xb31 X10 + Xb32 X11 + Xb33 X12 + Xb34 X13 + Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39 X18$$

$$b15(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13 + Xb15 X14 + Xb16 X15 + Xb17 X16 + Xb18 X17 + Xb19 X18 + b16 (Xb31 X10 + Xb32 X11 + Xb33 X12 + Xb34 X13 + Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39 X18$$

$$b17(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13 + Xb15 X14 + Xb16 X15 + Xb17 X16 + Xb18 X17 + Xb19 X18 + b18 (Xb31 X10 + Xb32 X11 + Xb33 X12 + Xb34 X13 + Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39 X18$$

setting

\*\*\*\*\*

$b1 Xb21 + b2 Xb31 = Xa1,$	$b3 Xb21 + b4 Xb31 = Xa10,$	$b5 Xb21 + b6 Xb31 = Xa19,$
$b1 Xb22 + b2 Xb32 = Xa2,$	$b3 Xb22 + b4 Xb32 = Xa11,$	$b5 Xb22 + b6 Xb32 = Xa20,$
$b1 Xb23 + b2 Xb33 = Xa3,$	$b3 Xb23 + b4 Xb33 = Xa12,$	$b5 Xb23 + b6 Xb33 = Xa21,$
$b1 Xb24 + b2 Xb34 = Xa4,$	$b3 Xb24 + b4 Xb34 = Xa13,$	$b5 Xb24 + b6 Xb34 = Xa22,$
$b1 Xb25 + b2 Xb35 = Xa5,$	$b3 Xb25 + b4 Xb35 = Xa14,$	$b5 Xb25 + b6 Xb35 = Xa23,$
$b1 Xb26 + b2 Xb36 = Xa6,$	$b3 Xb26 + b4 Xb36 = Xa15,$	$b5 Xb26 + b6 Xb36 = Xa24,$
$b1 Xb27 + b2 Xb37 = Xa7,$	$b3 Xb27 + b4 Xb37 = Xa16,$	$b5 Xb27 + b6 Xb37 = Xa25,$
$b1 Xb28 + b2 Xb38 = Xa8,$	$b3 Xb28 + b4 Xb38 = Xa17,$	$b5 Xb28 + b6 Xb38 = Xa26,$
$b1 Xb29 + b2 Xb39 = Xa9,$	$b3 Xb29 + b4 Xb39 = Xa18,$	$b5 Xb29 + b6 Xb39 = Xa27,$

$b9 Xb21 + b10 Xb31 = Xa37,$	$b11 Xb11 + b12 Xb31 = Xa46,$	$b7 Xb21 + b8 Xb31 = Xa28,$
$b9 Xb22 + b10 Xb32 = Xa38,$	$b11 Xb12 + b12 Xb32 = Xa47,$	$b7 Xb22 + b8 Xb32 = Xa29,$
$b9 Xb23 + b10 Xb33 = Xa39,$	$b11 Xb13 + b12 Xb33 = Xa48,$	$b7 Xb23 + b8 Xb33 = Xa30,$
$b9 Xb24 + b10 Xb34 = Xa40,$	$b11 Xb14 + b12 Xb34 = Xa49,$	$b7 Xb24 + b8 Xb34 = Xa31,$
$b9 Xb25 + b10 Xb35 = Xa41,$	$b11 Xb15 + b12 Xb35 = Xa50,$	$b7 Xb25 + b8 Xb35 = Xa32,$
$b9 Xb26 + b10 Xb36 = Xa42,$	$b11 Xb16 + b12 Xb36 = Xa51,$	$b7 Xb26 + b8 Xb36 = Xa33,$
$b9 Xb27 + b10 Xb37 = Xa43,$	$b11 Xb17 + b12 Xb37 = Xa52,$	$b7 Xb27 + b8 Xb37 = Xa34,$
$b9 Xb28 + b10 Xb38 = Xa44,$	$b11 Xb18 + b12 Xb38 = Xa53,$	$b7 Xb28 + b8 Xb38 = Xa35,$
$b9 Xb29 + b10 Xb39 = Xa45,$	$b11 Xb19 + b12 Xb39 = Xa54,$	$b7 Xb29 + b8 Xb39 = Xa36,$

$b13 Xb11 + b14 Xb31 = Xa55,$	$b15 Xb11 + b16 Xb31 = Xa64,$	$b17 Xb11 + b18 Xb31 = Xa73,$
$b13 Xb12 + b14 Xb32 = Xa56,$	$b15 Xb12 + b16 Xb32 = Xa65,$	$b17 Xb12 + b18 Xb32 = Xa74,$
$b13 Xb13 + b14 Xb33 = Xa57,$	$b15 Xb13 + b16 Xb33 = Xa66,$	$b17 Xb13 + b18 Xb33 = Xa75,$
$b13 Xb14 + b14 Xb34 = Xa58,$	$b15 Xb14 + b16 Xb34 = Xa67,$	$b17 Xb14 + b18 Xb34 = Xa76,$
$b13 Xb15 + b14 Xb35 = Xa59,$	$b15 Xb15 + b16 Xb35 = Xa68,$	$b17 Xb15 + b18 Xb35 = Xa77,$
$b13 Xb16 + b14 Xb36 = Xa60,$	$b15 Xb16 + b16 Xb36 = Xa69,$	$b17 Xb16 + b18 Xb36 = Xa78,$
$b13 Xb17 + b14 Xb37 = Xa61,$	$b15 Xb17 + b16 Xb37 = Xa70,$	$b17 Xb17 + b18 Xb37 = Xa79,$
$b13 Xb18 + b14 Xb38 = Xa62,$	$b15 Xb18 + b16 Xb38 = Xa71,$	$b17 Xb18 + b18 Xb38 = Xa80,$
$b13 Xb19 + b14 Xb39 = Xa63,$	$b15 Xb19 + b16 Xb39 = Xa72,$	$b17 Xb19 + b18 Xb39 = Xa81,$

B2 u =

$$Xa1 X10 + Xa2 X11 + Xa3 X12 + Xa4 X13 + Xa5 X14 + Xa6 X15 + Xa7 X16 + Xa8 X17 + Xa9 X18$$

$$Xa10 X10 + Xa11 X11 + Xa12 X12 + Xa13 X13 + Xa14 X14 + Xa15 X15 + Xa16 X16 + Xa17 X17 + Xa18 X18$$

$$Xa19 X10 + Xa20 X11 + Xa21 X12 + Xa22 X13 + Xa23 X14 + Xa24 X15 + Xa25 X16 + Xa26 X17 + Xa27 X18$$

$$Xa28 X10 + Xa29 X11 + Xa30 X12 + Xa31 X13 + Xa32 X14 + Xa33 X15 + Xa34 X16 + Xa35 X17 + Xa36 X18$$

$$Xa37 X10 + Xa38 X11 + Xa39 X12 + Xa40 X13 + Xa41 X14 + Xa42 X15 + Xa43 X16 + Xa44 X17 + Xa45 X18$$

$$Xa46 X10 + Xa47 X11 + Xa48 X12 + Xa49 X13 + Xa50 X14 + Xa51 X15 + Xa52 X16 + Xa53 X17 + Xa54 X18$$

$$Xa55 X10 + Xa56 X11 + Xa57 X12 + Xa58 X13 + Xa59 X14 + Xa60 X15 + Xa61 X16 + Xa62 X17 + Xa63 X18$$

$$Xa64 X10 + Xa65 X11 + Xa66 X12 + Xa67 X13 + Xa68 X14 + Xa69 X15 + Xa70 X16 + Xa71 X17 + Xa72 X18$$

$$Xa73 X10 + Xa74 X11 + Xa75 X12 + Xa76 X13 + Xa77 X14 + Xa78 X15 + Xa79 X16 + Xa80 X17 + Xa81 X18$$

\*\*\*Observe 9 states ---

C2t ( y - C2 X(10-18\*)=

$$C2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$$C2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

Y(9,9) C2T ( y - C2 X(10-18\* )

Y11	Y12	Y13	Y14	Y15	Y16	Y17	Y18	Y19	y1 - x10
Y12	Y22	Y23	Y24	Y25	Y26	Y27	Y28	Y29	y2 - x11
Y13	Y23	Y33	Y34	Y35	Y36	Y37	Y38	Y39	y3 - x12
= Y14	Y24	Y34	Y44	Y45	Y46	Y47	Y48	Y49	y4 - x13
Y15	Y25	Y35	Y45	Y55	Y56	Y57	Y58	Y59	y5 - x14
Y16	Y26	Y36	Y46	Y56	Y66	Y67	Y68	Y69	y6 - x15
Y17	Y27	Y37	Y47	Y57	Y67	Y77	Y78	Y79	y7 - x16
Y18	Y28	Y38	Y48	Y58	Y68	Y78	Y88	Y89	y8 - x17
Y19	Y29	Y39	Y49	Y59	Y69	Y79	Y89	Y99	y9 - x18

=

$$Y11(y1 - x10) + Y12(y2 - x11) + Y13(y3 - x12) + Y14(y4 - x13) + Y15(y5 - x14) + Y16(y6 - x15) + Y17(y7 - x16) + Y18(y8 - x17) + Y19(y9 - x18) + Y22(y2 - x11) + Y23(y3 - x12) + Y24(y4 - x13) + Y25(y5 - x14) + Y26(y6 - x15) + Y27(y7 - x16) + Y28(y8 - x17) + Y29(y9 - x18) + Y33(y3 - x12) + Y34(y4 - x13) + Y35(y5 - x14) + Y36(y6 - x15) + Y37(y7 - x16) + Y38(y8 - x17) + Y39(y9 - x18) + Y44(y4 - x13) + Y45(y5 - x14) + Y46(y6 - x15) + Y47(y7 - x16) + Y48(y8 - x17) + Y49(y9 - x18) + Y55(y5 - x14) + Y56(y6 - x15) + Y57(y7 - x16) + Y58(y8 - x17) + Y59(y9 - x18) + Y66(y6 - x15) + Y67(y7 - x16) + Y68(y8 - x17) + Y69(y9 - x18) + Y77(y7 - x16) + Y78(y8 - x17) + Y79(y9 - x18) + Y88(y8 - x17) + Y89(y9 - x18)$$

= -

Y11	x10	+Y12	x11	+Y13	x12	+Y14	x13	+Y15	x14	+Y16	x15	+Y17	x16	+Y18	x17	+Y19	x18	+Y19	y9
Y12	x10	+Y22	x11	+Y23	x12	+Y24	x13	+Y25	x14	+Y26	x15	+Y27	x16	+Y28	x17	+Y29	x18	+Y29	y9
Y13	x10	+Y23	x11	+Y33	x12	+Y34	x13	+Y35	x14	+Y36	x15	+Y37	x16	+Y38	x17	+Y39	x18	+Y39	y9
Y14	x10	+Y24	x11	+Y34	x12	+Y44	x13	+Y45	x14	+Y46	x15	+Y47	x16	+Y48	x17	+Y49	x18	+Y49	y9
Y15	x10	+Y25	x11	+Y35	x12	+Y45	x13	+Y55	x14	+Y56	x15	+Y57	x16	+Y58	x17	+Y59	x18	+Y59	y9
Y16	x10	+Y26	x11	+Y36	x12	+Y46	x13	+Y56	x14	+Y66	x15	+Y67	x16	+Y68	x17	+Y69	x18	+Y69	y9
Y17	x10	+Y27	x11	+Y37	x12	+Y47	x13	+Y57	x14	+Y67	x15	+Y77	x16	+Y78	x17	+Y79	x18	+Y79	y9
Y18	x10	+Y28	x11	+Y38	x12	+Y48	x13	+Y58	x14	+Y68	x15	+Y78	x16	+Y88	x17	+Y89	x18	+Y89	y9
Y19	x10	+Y29	x11	+Y39	x12	+Y49	x13	+Y59	x14	+Y69	x15	+Y79	x16	+Y89	x17	+Y99	x18	+Y89	y9
Y11	y1	+Y12	y2	+Y13	y3	+Y14	y4	+Y15	y5	+Y16	y6	+Y17	y7	+Y18	y8	+Y19	y9		
Y12	y1	+Y22	y2	+Y23	y3	+Y24	y4	+Y25	y5	+Y26	y6	+Y27	y7	+Y28	y8	+Y29	y9		
Y13	y1	+Y23	y2	+Y33	y3	+Y34	y4	+Y35	y5	+Y36	y6	+Y37	y7	+Y38	y8	+Y39	y9		
Y14	y1	+Y24	y2	+Y34	y3	+Y44	y4	+Y45	y5	+Y46	y6	+Y47	y7	+Y48	y8	+Y49	y9		
Y15	y1	+Y25	y2	+Y35	y3	+Y45	y4	+Y55	y5	+Y56	y6	+Y57	y7	+Y58	y8	+Y59	y9		
Y16	y1	+Y26	y2	+Y36	y3	+Y46	y4	+Y56	y5	+Y66	y6	+Y67	y7	+Y68	y8	+Y69	y9		
Y17	y1	+Y27	y2	+Y37	y3	+Y47	y4	+Y57	y5	+Y67	y6	+Y77	y7	+Y78	y8	+Y79	y9		
Y18	y1	+Y28	y2	+Y38	y3	+Y48	y4	+Y58	y5	+Y68	y6	+Y78	y7	+Y88	y8	+Y89	y9		
Y19	y1	+Y29	y2	+Y39	y3	+Y49	y4	+Y59	y5	+Y69	y6	+Y79	y7	+Y89	y8	+Y99	y9		

	%-----		%-----
Ob1 = ( a11 - Xa1 - Y(1,1) )	Ob28=( 0 - Xa28 - Y(1,4) )	Ob55=( 0 - Xa55 - Y(1,7) )	
Ob2 = ( a12 - Xa2 - Y(1,2) )	Ob29=( 0 - Xa29 - Y(2,4) )	Ob56=( 0 - Xa56 - Y(2,7) )	
Ob3 = ( a13 - Xa3 - Y(1,3) )	Ob30=( a43 - Xa30 - Y(3,4) )	Ob57=( 0 - Xa57 - Y(3,7) )	
Ob4 = ( a14 - Xa4 - Y(1,4) )	Ob31=( 0 - Xa31 - Y(4,4) )	Ob58=( a74 - Xa58 - Y(4,7) )	
Ob5 = ( a15 - Xa5 - Y(1,5) )	Ob32=( a45 - Xa32 - Y(4,5) )	Ob59=( 0 - Xa59 - Y(5,7) )	
Ob6 = ( a16 - Xa6 - Y(1,6) )	Ob33=( 0 - Xa33 - Y(4,6) )	Ob60=( a76 - Xa60 - Y(6,7) )	
Ob7 = ( a17 - Xa7 - Y(1,7) )	Ob34=( a47 - Xa34 - Y(4,7) )	Ob61=( 0 - Xa61 - Y(7,7) )	
Ob8 = ( a18 - Xa8 - Y(1,8) )	Ob35=( 0 - Xa35 - Y(4,8) )	Ob62=( a78 - Xa62 - Y(7,8) )	
Ob9 = ( a19 - Xa9 - Y(1,9) )	Ob36=( 0 - Xa36 - Y(4,9) )	Ob63=( 0 - Xa63 - Y(7,9) )	
Ob1s = -Y(1,1)	Ob16s = -Y(1,4)	Ob31s = -Y(1,7)	
Ob2s = -Y(1,2)	Ob17s = -Y(2,4)	Ob32s = -Y(2,7)	
Ob3s = -Y(1,3)	Ob18s = -Y(3,4)	Ob33s = -Y(3,7)	
Ob4s = -Y(1,4)	Ob19s = -Y(4,4)	Ob34s = -Y(4,7)	
Ob5s = -Y(1,5)	Ob20s = -Y(4,5)	Ob35s = -Y(5,7)	
Ob1ss = -Y(1,6)	Ob16ss = -Y(4,6)	Ob31ss = -Y(6,7)	
Ob2ss = -Y(1,7)	Ob17ss = -Y(4,7)	Ob32ss = -Y(7,7)	
Ob3ss = -Y(1,8)	Ob18ss = -Y(4,8)	Ob33ss = -Y(7,8)	
Ob4ss = -Y(1,9)	Ob19ss = -Y(4,9)	Ob34ss = -Y(7,9)	
%-----	%-----	%-----	
Ob10=( a21 - Xa10 - Y(1,2) )	Ob37=( 0 - Xa37 - Y(1,5) )	Ob64=( 0 - Xa64 - Y(1,8) )	
Ob11=( 0 - Xa11 - Y(2,2) )	Ob38=( 0 - Xa38 - Y(2,5) )	Ob65=( 0 - Xa65 - Y(2,8) )	
Ob12=( a23 - Xa12 - Y(2,3) )	Ob39=( 0 - Xa39 - Y(3,5) )	Ob66=( a83 - Xa66 - Y(3,8) )	
Ob13=( 0 - Xa13 - Y(2,4) )	Ob40=( a54 - Xa40 - Y(4,5) )	Ob67=( 0 - Xa67 - Y(4,8) )	
Ob14=( 0 - Xa14 - Y(2,5) )	Ob41=( 0 - Xa41 - Y(5,5) )	Ob68=( 0 - Xa68 - Y(5,8) )	
Ob15=( 0 - Xa15 - Y(2,6) )	Ob42=( a56 - Xa42 - Y(5,6) )	Ob69=( 0 - Xa69 - Y(6,8) )	
Ob16=( 0 - Xa16 - Y(2,7) )	Ob43=( 0 - Xa43 - Y(5,7) )	Ob70=( a87 - Xa70 - Y(7,8) )	
Ob17=( 0 - Xa17 - Y(2,8) )	Ob44=( 0 - Xa44 - Y(5,8) )	Ob71=( 0 - Xa71 - Y(8,8) )	
Ob18=( a29 - Xa18 - Y(2,9) )	Ob45=( 0 - Xa45 - Y(5,9) )	Ob72=( a89 - Xa72 - Y(8,9) )	
Ob6s = -Y(1,2)	Ob21s = -Y(1,5)	Ob36s = -Y(1,8)	
Ob7s = -Y(2,2)	Ob22s = -Y(2,5)	Ob37s = -Y(2,8)	
Ob8s = -Y(2,3)	Ob23s = -Y(3,5)	Ob38s = -Y(3,8)	
Ob9s = -Y(2,4)	Ob24s = -Y(4,5)	Ob39s = -Y(4,8)	
Ob10s = -Y(2,5)	Ob25s = -Y(5,5)	Ob40s = -Y(5,8)	
Ob6ss = -Y(2,6)	Ob21ss = -Y(5,6)	Ob36ss = -Y(6,8)	
Ob7ss = -Y(2,7)	Ob22ss = -Y(5,7)	Ob37ss = -Y(7,8)	
Ob8ss = -Y(2,8)	Ob23ss = -Y(5,8)	Ob38ss = -Y(8,8)	
Ob9ss = -Y(2,9)	Ob24ss = -Y(5,9)	Ob39ss = -Y(8,9)	
%-----	%-----	%-----	
Ob19=( 0 - Xa19 - Y(1,3) )	Ob46=( 0 - Xa46 - Y(1,6) )	Ob73=( a91 - Xa73 - Y(1,9) )	
Ob20=( a32 - Xa20 - Y(2,3) )	Ob47=( 0 - Xa47 - Y(2,6) )	Ob74=( a92 - Xa74 - Y(2,9) )	
Ob21=( 0 - Xa21 - Y(3,3) )	Ob48=( 0 - Xa48 - Y(3,6) )	Ob75=( a93 - Xa75 - Y(3,9) )	
Ob22=( a34 - Xa22 - Y(3,4) )	Ob49=( 0 - Xa49 - Y(4,6) )	Ob76=( a94 - Xa76 - Y(4,9) )	
Ob23=( 0 - Xa23 - Y(3,5) )	Ob50=( a65 - Xa50 - Y(5,6) )	Ob77=( a95 - Xa77 - Y(5,9) )	
Ob24=( 0 - Xa24 - Y(3,6) )	Ob51=( 0 - Xa51 - Y(6,6) )	Ob78=( a96 - Xa78 - Y(6,9) )	
Ob25=( 0 - Xa25 - Y(3,7) )	Ob52=( a67 - Xa52 - Y(6,7) )	Ob79=( a97 - Xa79 - Y(7,9) )	
Ob26=( a38 - Xa26 - Y(3,8) )	Ob53=( 0 - Xa53 - Y(6,8) )	Ob80=( a98 - Xa80 - Y(8,9) )	
Ob27=( 0 - Xa27 - Y(3,9) )	Ob54=( 0 - Xa54 - Y(6,9) )	Ob81=( a99 - Xa81 - Y(9,9) )	
Ob11s = -Y(1,3)	Ob26s = -Y(1,6)	Ob41s = -Y(1,9)	
Ob12s = -Y(2,3)	Ob27s = -Y(2,6)	Ob42s = -Y(2,9)	
Ob13s = -Y(3,3)	Ob28s = -Y(3,6)	Ob43s = -Y(3,9)	
Ob14s = -Y(3,4)	Ob29s = -Y(4,6)	Ob44s = -Y(4,9)	
Ob15s = -Y(3,5)	Ob30s = -Y(5,6)	Ob45s = -Y(5,9)	
Ob11ss = -Y(3,6)	Ob26ss = -Y(6,6)	Ob41ss = -Y(6,9)	
Ob12ss = -Y(3,7)	Ob27ss = -Y(6,7)	Ob42ss = -Y(7,9)	
Ob13ss = -Y(3,8)	Ob28ss = -Y(6,8)	Ob43ss = -Y(8,9)	
Ob14ss = -Y(3,9)	Ob29ss = -Y(6,9)	Ob44ss = -Y(9,9)	
		%-----	

$$\begin{aligned}
 \text{xdot}(1) &= a11*x(1) + a12*x(2) + a13*x(3) + a14*x(4) + a15*x(5) + a16*x(6) + a17*x(7) + a18*x(8) + a19*x(9) \\
 &\quad + Xa1*x(10) + Xa2*x(11) + Xa3*x(12) + Xa4*x(13) + Xa5*x(14) + Xa6*x(15) + Xa7*x(16) + Xa8*x(17) + Xa9*x(18) \\
 \text{xdot}(2) &= a21*x(1) + a23*x(3) + a29*x(9) \\
 &\quad + Xa10*x(10) + Xa11*x(11) + Xa12*x(12) + Xa13*x(13) + Xa14*x(14) + Xa15*x(15) + Xa16*x(16) + Xa17*x(17) + Xa18*x(18) \\
 \text{xdot}(3) &= a32*x(2) + a34*x(4) + a38*x(8) \\
 &\quad + Xa19*x(10) + Xa20*x(11) + Xa21*x(12) + Xa22*x(13) + Xa23*x(14) + Xa24*x(15) + Xa25*x(16) + Xa26*x(17) + Xa27*x(18) \\
 \text{xdot}(4) &= a43*x(3) + a45*x(5) + a47*a7 \\
 &\quad + Xa28*x(10) + Xa29*x(11) + Xa30*x(12) + Xa31*x(13) + Xa32*x(14) + Xa33*x(15) + Xa34*x(16) + Xa35*x(17) + Xa36*x(18) \\
 \text{xdot}(5) &= a54*x(4) + a56*x(6) \\
 &\quad + Xa37*x(10) + Xa38*x(11) + Xa39*x(12) + Xa40*x(13) + Xa41*x(14) + Xa42*x(15) + Xa43*x(16) + Xa44*x(17) + Xa45*x(18) \\
 \text{xdot}(6) &= a65*x(5) + a67*x(7) \\
 &\quad + Xa46*x(10) + Xa47*x(11) + Xa48*x(12) + Xa49*x(13) + Xa50*x(14) + Xa51*x(15) + Xa52*x(16) + Xa53*x(17) + Xa54*x(18) \\
 \text{xdot}(7) &= a74*x(4) + a76*x(6) + a78*x(8) \\
 &\quad + Xa55*x(10) + Xa56*x(11) + Xa57*x(12) + Xa58*x(13) + Xa59*x(14) + Xa60*x(15) + Xa61*x(16) + Xa62*x(17) + Xa63*x(18) \\
 \text{xdot}(8) &= a83*x(3) + a87*x(7) + a89*x(9) \\
 &\quad + Xa64*x(10) + Xa65*x(11) + Xa66*x(12) + Xa67*x(13) + Xa68*x(14) + Xa69*x(15) + Xa70*x(16) + Xa71*x(17) + Xa72*x(18) \\
 \text{xdot}(9) &= a91*x(1) + a92*x(2) + a93*x(3) + a94*x(4) + a95*x(5) + a96*x(6) + a97*x(7) + a98*x(8) + a99*x(9) \\
 &\quad + Xa73*x(10) + Xa74*x(11) + Xa75*x(12) + Xa76*x(13) + Xa77*x(14) + Xa78*x(15) + Xa79*x(16) + Xa80*x(17) + Xa81*x(18) \\
 \text{xdot}(10) &= Ob1*x(10) + Ob2*x(11) + Ob3*x(12) + Ob4*x(13) + Ob5*x(14) + Ob6*x(15) + Ob7*x(16) + Ob8*x(17) + Ob9*x(18) \\
 &\quad + Ob1s*x(1) + Ob2s*x(2) + Ob3s*x(3) + Ob4s*x(4) + Ob5s*x(5) + Ob1ss*x(6) + Ob2ss*x(7) + Ob3ss*x(8) + Ob4ss*x(9) \\
 \text{xdot}(11) &= Ob10*x(10) + Ob11*x(11) + Ob12*x(12) + Ob13*x(13) + Ob14*x(14) + Ob15*x(15) + Ob16*x(16) + Ob17*x(17) + Ob18*x(18) \\
 &\quad + Ob6s*x(1) + Ob7s*x(2) + Ob8s*x(3) + Ob9s*x(4) + Ob10s*x(5) + Ob6ss*x(6) + Ob7ss*x(7) + Ob8ss*x(8) + Ob9ss*x(9) \\
 \text{xdot}(12) &= Ob19*x(10) + Ob20*x(11) + Ob21*x(12) + Ob22*x(13) + Ob23*x(14) + Ob24*x(15) + Ob25*x(16) + Ob26*x(17) \\
 &\quad + Ob27*x(18) + Ob11s*x(1) + Ob12s*x(2) + Ob13s*x(3) + Ob14s*x(4) + Ob15s*x(5) + Ob11ss*x(6) + Ob12ss*x(7) \\
 &\quad + Ob13ss*x(8) + Ob14ss*x(9) \\
 \text{xdot}(13) &= Ob28*x(10) + Ob29*x(11) + Ob30*x(12) + Ob31*x(13) + Ob32*x(14) + Ob33*x(15) + Ob34*x(16) + Ob35*x(17) + Ob36*x(18) \\
 &\quad + Ob16s*x(1) + Ob17s*x(2) + Ob18s*x(3) + Ob19s*x(4) + Ob20s*x(5) + Ob16ss*x(6) + Ob17ss*x(7) + Ob18ss*x(8) + Ob19ss*x(9) \\
 \text{xdot}(14) &= Ob37*x(10) + Ob38*x(11) + Ob39*x(12) + Ob40*x(13) + Ob41*x(14) + Ob42*x(15) + Ob43*x(16) \\
 &\quad + Ob44*x(17) + Ob45*x(18) + Ob21s*x(1) + Ob22s*x(2) + Ob23s*x(3) + Ob24s*x(4) + Ob25s*x(5) + Ob21ss*x(6) \\
 &\quad + Ob22ss*x(7) + Ob23ss*x(8) + Ob24ss*x(9) \\
 \text{xdot}(15) &= Ob46*x(10) + Ob47*x(11) + Ob48*x(12) + Ob49*x(13) + Ob50*x(14) + Ob51*x(15) + Ob52*x(16) + Ob53*x(17) + Ob54*x(18) \\
 &\quad + Ob26s*x(1) + Ob27s*x(2) + Ob28s*x(3) + Ob29s*x(4) + Ob30s*x(5) + Ob26ss*x(6) + Ob27ss*x(7) + Ob28ss*x(8) + Ob29ss*x(9) \\
 \text{xdot}(16) &= Ob55*x(10) + Ob56*x(11) + Ob57*x(12) + Ob58*x(13) + Ob59*x(14) + Ob60*x(15) + Ob61*x(16) + Ob62*x(17) + Ob63*x(18) \\
 &\quad + Ob31s*x(1) + Ob32s*x(2) + Ob33s*x(3) + Ob34s*x(4) + Ob35s*x(5) + Ob31ss*x(6) + Ob32ss*x(7) + Ob33ss*x(8) + Ob34ss*x(9) \\
 \text{xdot}(17) &= Ob64*x(10) + Ob65*x(11) + Ob66*x(12) + Ob67*x(13) + Ob68*x(14) + Ob69*x(15) + Ob70*x(16) + Ob71*x(17) + Ob72*x(18) \\
 &\quad + Ob36s*x(1) + Ob37s*x(2) + Ob38s*x(3) + Ob39s*x(4) + Ob40s*x(5) + Ob36ss*x(6) + Ob37ss*x(7) + Ob38ss*x(8) + Ob39ss*x(9) \\
 \text{xdot}(18) &= Ob73*x(10) + Ob74*x(11) + Ob75*x(12) + Ob76*x(13) + Ob77*x(14) + Ob78*x(15) + Ob79*x(16) + Ob80*x(17) + Ob81*x(18) \\
 &\quad + Ob41s*x(1) + Ob42s*x(2) + Ob43s*x(3) + Ob44s*x(4) + Ob45s*x(5) + Ob41ss*x(6) + Ob42ss*x(7) + Ob43ss*x(8) + Ob44ss*x(9)
 \end{aligned}$$

To close the loop, we set the negative feed back as

$$\begin{aligned}
 y1 &= -x1, \\
 y2 &= -x2 \\
 y3 &= -x3, \\
 y4 &= -x4 \\
 y5 &= -x5, \\
 y6 &= -x6 \\
 y7 &= -x7, \\
 y8 &= -x8 \\
 y9 &= -x9,
 \end{aligned}$$

We can obtain the coefficients Obn and Obsn

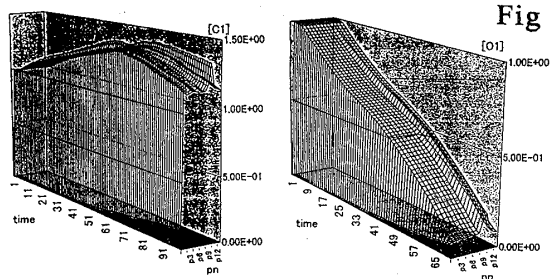


Fig 5

## 2. Results.

Fig 5 shows the temporal changes in [C1] and [O1] with changes in weighting coefficients for the control inputs un. Significant changes can be observed at particular pn. The present evaluation when extended will be available for predicting the noise filtering function of biomembranes.

## 3. Reference

1. Matkes.T.N and Jones.W. J.Gen. Phys. vol 99. pp 367. 1992.