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Method of Matrices Operations in H2 Control for Calcium Ion Channel on the Biological Membrane as a Closed Circuit.

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あらまし

I have proposed an h2 control principle for bio chemical noise filtering function of the calcium in channel on the excitable cellular membrane. The Calcium channel is composed of four identical subunits. Each of which contains a helical segment which contains a lot of electrical charge that acts as a membrane voltage sensor. The opening and closing of the channel pore are facilitated by the activating positionings of the voltage sensor. The temporal changes in the system were described by ten differential equations under the condition that minimizes the 2 norm of the transfer function of the system from the noise input to the output. The computed temporal changes in the open and closed states are significantly influenced by the changes in the amounts of the control inputs. The present methods, when extended will be available for evaluating the filtering function of the bio membranes.

和文キーワード Bio membrane, calcium in, Channel, Subunits, Voltage sensor, H2 control, Noise, 2 norm.

閉回路としてのカルシウムイオンチャンネルのH2制御

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Abstract

カルシウムイオンを選択的に通過させるカルシウムイオンチャンネルの機能特性を雑音フィルターの視点からH2制御を用いて解析する方法を提唱した。カルシウムイオンチャンネルは4個の相同性の高いサブユニットから構成されている。また膜電位感受性を有するタンパク分子がそれぞれのサブユニットに付属し、その空間内の位置が変化することでチャンネル開閉が加速される。本研究では10個のチャンネル構造を10個の状態方程式で表示し、雑音が outputされるまでの系の伝達関数の2ノルムを最少にする場合のチャンネルの状態の過渡的状況を数値計算で決定した。制御入力の変化によって開状態、閉状態のチャンネルの時間経過を大きく影響された。本研究を発展させることで生体膜チャンネルの生化学的雑音低減効果を評価できる可能性を示唆した。

英文 key words 生体膜、カルシウムイオン、チャンネル、H2制御、雑音、伝達関数 2ノルム

1. Introduction.

Calcium channel (Fig 1) on the excitable membrane filters only Calcium ion though there are a lot of agonist and antagonist that compete the channel with Calcium ion. Hence, the mechanism can be described by the H2 control principle. The dynamical action of the Calcium channel is characterized by four identical subunits (Fig 2) that act concertedly. The channel opening and closing are strongly influenced by a particular segment named S4 (Fig 3) which has a high voltage sensing property in each subunits. S4 contains a lot of charges on its surface. When it takes the activating position in the subunit, the transitions among the open states are facilitated. By the spatial consideration of the activating positionings of the voltage sensor, we have ten conformations of one Calcium channel. (Fig 4-a and Fig 4-b).

In the present work, we present a detailed matrix expansion for computing the H2 controlled temporal change of the amounts of the Calcium channel states.

2. Mathematical method.

The state equations for these ten conformation states are given by linear combination of weighted control inputs.

Fig 1

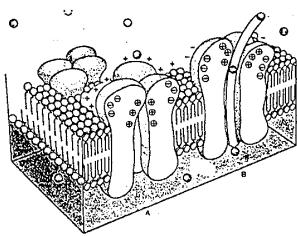


Fig 2

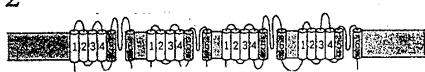


Fig 3

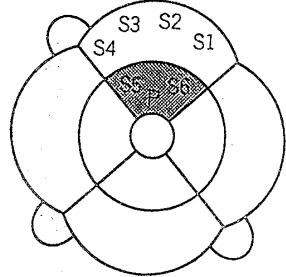
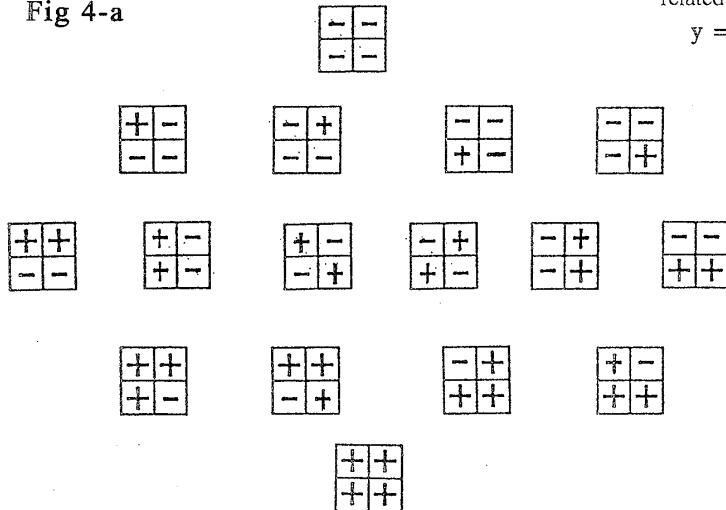


Fig 4-a



$$\begin{aligned} \partial C_0 / \partial t &= k_c C_1 + k_L / f_4 O_0 - (4 k_c + k_L f_4) C_0 \\ &\quad + p_9' u_3 + p_1' u_1 \quad \dots(1) \\ \partial C_1 / \partial t &= 4 k_c C_0 + 2 k_c C_2 + k_L / f_3 O_1 - (k_c + 3 k_c + k_L f_3) C_1 + p_1 u_1 + p_{10}' u_3 + p_2' u_1 \quad \dots(2) \\ \partial C_2 / \partial t &= 3 k_c C_1 + 3 k_c C_3 + k_L / f_2 O_2 - (2 k_c + 2 k_c + k_L f_2) C_2 + p_2 u_1 + p_{11}' u_3 + p_3' u_1 \quad \dots(3) \\ \partial C_3 / \partial t &= 2 k_c C_2 + 4 k_c C_4 + k_L / f_1 O_3 - (3 k_c + k_c + k_L f_1) C_3 + p_3 u_1 + p_{12}' u_3 + p_4' u_1 \quad \dots(4) \\ \partial C_4 / \partial t &= k_c C_3 + k_L O_4 - (4 k_c + k_L) C_4 \\ &\quad + p_4 u_1 + p_{13}' u_3 \quad \dots(5) \\ \partial O_0 / \partial t &= f_4 k_L C_0 + k_c f_1 O_1 - (k_L / f_4 + 4 k_c / f_1) O_0 \\ &\quad + p_9 u_3 + p_5' u_2 \quad \dots(6) \\ \partial O_1 / \partial t &= 4 k_c / f_1 O_0 + k_L f_3 C_1 + 2 k_c f_2 O_2 \\ &\quad - (k_c f_1 + k_L / f_3 + 3 k_c / f_2) O_1 + p_{10} u_3 + p_6' u_2 \quad \dots(7) \\ \partial O_2 / \partial t &= 3 k_c / f_2 O_1 + k_L f_2 C_2 + 3 k_c f_3 O_3 \\ &\quad - (2 f_2 k_c + k_L / f_2 + 2 k_c / f_3) O_2 + p_{11} u_3 + p_7' u_2 \quad \dots(8) \\ \partial O_3 / \partial t &= 2 k_c / f_3 O_2 + k_L f_3 C_3 + 4 k_c f_4 O_4 - (3 k_c f_3 + k_L / f_3 + k_c / f_4) O_3 + p_7 u_2 + p_{12} u_3 + p_8' u_2 \quad \dots(9) \\ \partial O_4 / \partial t &= k_c / f_4 O_3 + k_L C_4 - (4 k_c f_4 + k_L) O_4 \\ &\quad + p_8 u_2 + p_{13} u_3 \quad \dots(10) \end{aligned}$$

The vector form

$$\partial \mathbf{x}'(t) / \partial t = \mathbf{A} \mathbf{x} + \mathbf{B}_1 \mathbf{w} + \mathbf{B}_2 \mathbf{u}$$

Vector form of the equation for the estimator \mathbf{Z}

$$\mathbf{Z} = \mathbf{C}_1 \mathbf{x} + \mathbf{D}_{12} \mathbf{u}$$

Vector form of the equation for the observer output \mathbf{y}

$$\mathbf{y} = \mathbf{C}_2 \mathbf{x} + \mathbf{D}_{21} \mathbf{w}$$

The vector for of the optimized control \mathbf{u}^* is given by the product of \mathbf{B}_2 , \mathbf{X} and \mathbf{x}^*

$$\mathbf{u}^* = -\mathbf{B}_2 \mathbf{T} \mathbf{X} \mathbf{x}^*$$

where \mathbf{x}^* is the state vector of the observers and \mathbf{T} denotes transpose.

$\mathbf{x}^* \mathbf{T} = [x_{10}, x_{11}, x_{12}, x_{13}, x_{14}, x_{15}, x_{16}, x_{17}, x_{18}]^T$ which correspond to state variables. \mathbf{X} is the solution of related algebraic Riccati equation.

$$\mathbf{A} \mathbf{T} \mathbf{X} + \mathbf{X} \mathbf{A} - \mathbf{X} \mathbf{B}_2 \mathbf{B}_2 \mathbf{T} \mathbf{X} + \mathbf{C}_1 \mathbf{T} \mathbf{C}_1 = 0$$

The vector equation of observer \mathbf{x}^* is given by

$\partial \mathbf{x}^* / \partial t = \mathbf{A} \mathbf{x}^* + \mathbf{B}_2 \mathbf{u} + \mathbf{Y} \mathbf{C}_2 \mathbf{T} (\mathbf{y} - \mathbf{C}_2 \mathbf{x}^*)$ where \mathbf{Y} is the solution of adjoint algebraic Riccati equation

$$\mathbf{A} \mathbf{Y} + \mathbf{Y} \mathbf{A} \mathbf{T} - \mathbf{Y} \mathbf{C}_2 \mathbf{T} \mathbf{C}_2 \mathbf{Y} + \mathbf{B}_1 \mathbf{B}_1 \mathbf{T} = 0$$

To close the feed back loop of the system, \mathbf{y} can be related to state variable \mathbf{x} by

$$\begin{aligned} \mathbf{y} &= \mathbf{x} \mathbf{d} - \mathbf{C}_2 \mathbf{x} \\ \mathbf{C}_0 &\xrightarrow[k_L/f^4]{f^4 k_L} \bigcirc \bigcirc O_0 \\ \mathbf{C}_1 &\xrightarrow[k_L/f^3]{f^3 k_L} \bigcirc \bigcirc O_1 \\ \mathbf{C}_2 &\xrightarrow[k_L/f^2]{f^2 k_L} \bigcirc \bigcirc O_2 \\ \mathbf{C}_3 &\xrightarrow[k_L/f]{f k_L} \bigcirc \bigcirc O_3 \\ \mathbf{C}_4 &\xrightarrow[k_L]{k_L} \bigcirc \bigcirc O_4 \end{aligned}$$

Fig 4-b

$A = [\begin{matrix} a_{11} & a_{12} & a_{13} & a_{14} & a_{15} & a_{16} & a_{17} & a_{18} & a_{19} \\ a_{21} & 0 & a_{23} & 0 & 0 & 0 & 0 & 0 & a_{29} \\ 0 & a_{32} & 0 & a_{34} & 0 & 0 & 0 & a_{38} & 0 \\ 0 & 0 & a_{43} & 0 & a_{45} & 0 & a_{47} & 0 & 0 \\ 0 & 0 & 0 & a_{54} & 0 & a_{56} & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & a_{65} & 0 & a_{67} & 0 & 0 \\ 0 & 0 & 0 & a_{74} & 0 & a_{76} & 0 & a_{78} & 0 \\ 0 & 0 & a_{83} & 0 & 0 & 0 & a_{87} & 0 & a_{89} \\ a_{91} & a_{92} & a_{93} & a_{94} & a_{95} & a_{96} & a_{97} & a_{98} & a_{99} \end{matrix}]$

 $\begin{matrix} 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \end{matrix}$

$B_2^T = \begin{matrix} b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}$

$$\begin{aligned} & b_{11} X_{36} + b_{13} X_{37} + b_{15} X_{38} + b_{17} X_{39} : X_{b13} \\ & b_1 X_{13} + b_3 X_{23} + b_5 X_{33} + b_7 X_{34} + b_9 X_{35} : X_{b23} \\ & b_2 X_{13} + b_4 X_{23} + b_6 X_{33} + b_8 X_{34} + b_{10} X_{35} \\ & + b_{12} X_{36} + b_{14} X_{37} + b_{16} X_{38} + b_{18} X_{39} : X_{b33} \end{aligned}$$

$$\begin{matrix} [X_{14} & X_{24} & X_{34} & X_{44} & X_{45} & X_{46} & X_{47} & X_{48} & X_{49}] \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}$$

$$\begin{aligned} & = \\ & b_{11} X_{46} + b_{13} X_{47} + b_{15} X_{48} + b_{17} X_{49} : X_{b14} \\ & b_1 X_{14} + b_3 X_{24} + b_5 X_{34} + b_7 X_{44} + b_9 X_{45} : X_{b24} \\ & b_2 X_{14} + b_4 X_{24} + b_6 X_{34} + b_8 X_{44} + b_{10} X_{45} \\ & + b_{12} X_{46} + b_{14} X_{47} + b_{16} X_{48} + b_{18} X_{49} : X_{b34} \end{aligned}$$

Matrix form of the Riccati solution X is

$X =$

$\begin{matrix} X_{11} & X_{12} & X_{13} & X_{14} & X_{15} & X_{16} & X_{17} & X_{18} & X_{19} \\ X_{12} & X_{22} & X_{23} & X_{24} & X_{25} & X_{26} & X_{27} & X_{28} & X_{29} \\ X_{13} & X_{23} & X_{33} & X_{34} & X_{35} & X_{36} & X_{37} & X_{38} & X_{39} \\ X_{14} & X_{24} & X_{34} & X_{44} & X_{45} & X_{46} & X_{47} & X_{48} & X_{49} \\ X_{15} & X_{25} & X_{35} & X_{45} & X_{55} & X_{56} & X_{57} & X_{58} & X_{59} \\ X_{16} & X_{26} & X_{36} & X_{46} & X_{56} & X_{66} & X_{67} & X_{68} & X_{69} \\ X_{17} & X_{27} & X_{37} & X_{47} & X_{57} & X_{67} & X_{77} & X_{78} & X_{79} \\ X_{18} & X_{28} & X_{38} & X_{48} & X_{58} & X_{68} & X_{78} & X_{88} & X_{89} \\ X_{19} & X_{29} & X_{39} & X_{49} & X_{59} & X_{69} & X_{79} & X_{89} & X_{99} \end{matrix}$

The control input is

$$u^* = -B_2^T X x^*$$

$B_2^T X =$

$[\begin{matrix} X_{11} & X_{12} & X_{13} & X_{14} & X_{15} & X_{16} & X_{17} & X_{18} & X_{19} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}]$

$=$

$b_{11} X_{16} + b_{13} X_{17} + b_{15} X_{18} + b_{17} X_{19} : X_{b11}$

$b_1 X_{11} + b_3 X_{12} + b_5 X_{13} + b_7 X_{14} + b_9 X_{15} : X_{b21}$

$b_2 X_{11} + b_4 X_{12} + b_6 X_{13} + b_8 X_{14} + b_{10} X_{15} +$

$+ b_{12} X_{16} + b_{14} X_{17} + b_{16} X_{18} + b_{18} X_{19} : X_{b31}$

$[\begin{matrix} X_{12} & X_{22} & X_{23} & X_{24} & X_{25} & X_{26} & X_{27} & X_{28} & X_{29} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}]$

$=$

$$\begin{matrix} [X_{15} & X_{25} & X_{35} & X_{45} & X_{55} & X_{56} & X_{57} & X_{58} & X_{59}] \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}$$

$$\begin{aligned} & = \\ & b_{11} X_{56} + b_{13} X_{57} + b_{15} X_{58} + b_{17} X_{59} : X_{b15} \\ & b_1 X_{15} + b_3 X_{25} + b_5 X_{35} + b_7 X_{45} + b_9 X_{55} : X_{b25} \\ & b_2 X_{15} + b_4 X_{25} + b_6 X_{35} + b_8 X_{45} + b_{10} X_{55} \\ & + b_{12} X_{56} + b_{14} X_{57} + b_{16} X_{58} + b_{18} X_{59} : X_{b35} \end{aligned}$$

$$\begin{matrix} [X_{16} & X_{26} & X_{36} & X_{46} & X_{56} & X_{66} & X_{67} & X_{68} & X_{69}] \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}$$

$$\begin{aligned} & = \\ & b_{11} X_{66} + b_{13} X_{67} + b_{15} X_{68} + b_{17} X_{69} : X_{b16} \\ & b_1 X_{16} + b_3 X_{26} + b_5 X_{36} + b_7 X_{46} + b_9 X_{56} : X_{b26} \\ & b_2 X_{16} + b_4 X_{26} + b_6 X_{36} + b_8 X_{46} + b_{10} X_{56} \\ & + b_{12} X_{66} + b_{14} X_{67} + b_{16} X_{68} + b_{18} X_{69} : X_{b36} \end{aligned}$$

$$\begin{matrix} [X_{17} & X_{27} & X_{37} & X_{47} & X_{57} & X_{67} & X_{77} & X_{78} & X_{79}] \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{matrix}$$

$$\begin{aligned} & = \\ & b_{11} X_{67} + b_{13} X_{77} + b_{15} X_{78} + b_{17} X_{79} : X_{b17} \\ & b_1 X_{17} + b_3 X_{27} + b_5 X_{37} + b_7 X_{47} + b_9 X_{57} : X_{b27} \\ & b_2 X_{17} + b_4 X_{27} + b_6 X_{37} + b_8 X_{47} + b_{10} X_{57} \\ & + b_{12} X_{67} + b_{14} X_{77} + b_{16} X_{78} + b_{18} X_{79} : X_{b37} \end{aligned}$$

$$\begin{bmatrix} X_{19} & X_{29} & X_{39} & X_{49} & X_{59} & X_{69} & X_{79} & X_{89} & X_{99} \\ 0 & 0 & 0 & 0 & 0 & b_{11} & b_{13} & b_{15} & b_{17} \\ b_1 & b_3 & b_5 & b_7 & b_9 & 0 & 0 & 0 & 0 \\ b_2 & b_4 & b_6 & b_8 & b_{10} & b_{12} & b_{14} & b_{16} & b_{18} \end{bmatrix}$$

$$= \\ b_{11} X_{69} + b_{13} X_{79} + b_{15} X_{89} + b_{17} X_{99} : X_{b19} \\ b_1 X_{19} + b_3 X_{29} + b_5 X_{39} + b_7 X_{49} + b_9 X_{59} : X_{b29} \\ b_2 X_{19} + b_4 X_{29} + b_6 X_{39} + b_8 X_{49} + b_{10} X_{59} \\ + b_{12} X_{69} + b_{14} X_{79} + b_{16} X_{89} + b_{18} X_{99} : X_{b39}$$

Then, we have

$$u = -B_2^T X x^*$$

$$= \\ [X_{b11} \quad X_{b12} \quad X_{b13} \quad X_{b14} \quad X_{b15} \quad X_{b16} \quad X_{b17} \quad X_{b18} \quad X_{b19} \\ X_{b21} \quad X_{b22} \quad X_{b23} \quad X_{b24} \quad X_{b25} \quad X_{b26} \quad X_{b27} \quad X_{b28} \quad X_{b29} \\ X_{b31} \quad X_{b32} \quad X_{b33} \quad X_{b34} \quad X_{b35} \quad X_{b36} \quad X_{b37} \quad X_{b38} \quad X_{b39}] \\ [x_{10} \ x_{11} \ x_{12} \ x_{13} \ x_{14} \ x_{15} \ x_{16} \ x_{17} \ x_{18}]^T \\ = \\ -[X_{b11} X_{10} + X_{b12} X_{11} + X_{b13} X_{12} + X_{b14} X_{13} + X_{b15} X_{14} + X_{b16} X_{15} + X_{b17} X_{16} + X_{b18} X_{17} + X_{b19} X_{18} \\ X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18} \\ X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}]$$

$$B_2 = \begin{bmatrix} 0 & b_1 & b_2 \\ 0 & b_3 & b_4 \\ 0 & b_5 & b_6 \\ 0 & b_7 & b_8 \\ 0 & b_9 & b_{10} \\ b_{11} & 0 & b_{12} \\ b_{13} & 0 & b_{14} \\ b_{15} & 0 & b_{16} \\ b_{17} & 0 & b_{18} \end{bmatrix}$$

$$B_2 u = \\ b_1 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\ + b_2 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\ b_3 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\ + b_4 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\ b_5 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\ + b_6 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\ b_7 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\ + b_8 (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\ b_9 (X_{b21} X_{10} + X_{b22} X_{11} + X_{b23} X_{12} + X_{b24} X_{13} + X_{b25} X_{14} + X_{b26} X_{15} + X_{b27} X_{16} + X_{b28} X_{17} + X_{b29} X_{18}) \\ + b_{10} (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18}) \\ b_{11} (X_{b11} X_{10} + X_{b12} X_{11} + X_{b13} X_{12} + X_{b14} X_{13} + X_{b15} X_{14} + X_{b16} X_{15} + X_{b17} X_{16} + X_{b18} X_{17} + X_{b19} X_{18}) \\ + b_{12} (X_{b31} X_{10} + X_{b32} X_{11} + X_{b33} X_{12} + X_{b34} X_{13} + X_{b35} X_{14} + X_{b36} X_{15} + X_{b37} X_{16} + X_{b38} X_{17} + X_{b39} X_{18})$$

b13(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13+ Xb15 X14+ Xb16 X15+ Xb17 X16 + Xb18 X17 + Xb19 X18
 + b14 (Xb31 X10 + Xb32 X11 + Xb33 X12+ Xb34 X13+ Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39
 X18

b15(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13+ Xb15 X14+ Xb16 X15+ Xb17 X16 + Xb18 X17 + Xb19 X18
 + b16 (Xb31 X10 + Xb32 X11 + Xb33 X12+ Xb34 X13+ Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39
 X18

b17(Xb11X10 + Xb12 X11 + Xb13 X12 + Xb14 X13+ Xb15 X14+ Xb16 X15+ Xb17 X16 + Xb18 X17 + Xb19 X18
 + b18 (Xb31 X10 + Xb32 X11 + Xb33 X12+ Xb34 X13+ Xb35 X14 + Xb36 X15 + Xb37 X16 + Xb38 X17 + Xb39
 X18

setting

b1 Xb21 + b2 Xb31 = Xa1,
 b1 Xb22 + b2 Xb32 = Xa2,
 b1 Xb23 + b2 Xb33 = Xa3,
 b1 Xb24 + b2 Xb34 = Xa4,
 b1 Xb25 + b2 Xb35 = Xa5,
 b1 Xb26 + b2 Xb36 = Xa6 ,
 b1 Xb27 + b2 Xb37 = Xa7
 b1 Xb28 + b2 Xb38 = Xa8
 b1 Xb29 + b2 Xb39 = Xa9

b3 Xb21 + b4 Xb31 = Xa10,
 b3 Xb22 + b4 Xb32 = Xa11,
 b3 Xb23 + b4 Xb33 = Xa12,
 b3 Xb24 + b4 Xb34 = Xa13,
 b3 Xb25 + b4 Xb35 = Xa14,
 b3 Xb26 + b4 Xb36 = Xa15 ,
 b3 Xb27 + b4 Xb37 = Xa16
 b3 Xb28 + b4 Xb38 = Xa17
 b3 Xb29 + b4 Xb39 = Xa18

b5 Xb21 + b6 Xb31 = Xa19,
 b5 Xb22 + b6 Xb32 = Xa20,
 b5 Xb23 + b6 Xb33 = Xa21,
 b5 Xb24 + b6 Xb34 = Xa22,
 b5 Xb25 + b6 Xb35 = Xa23,
 b5 Xb26 + b6 Xb36 = Xa24 ,
 b5 Xb27 + b6 Xb37 = Xa25
 b5 Xb28 + b6 Xb38 = Xa26
 b5 Xb29 + b6 Xb39 = Xa27

b9 Xb21 + b10 Xb31 = Xa37,
 b9 Xb22 + b10 Xb32 = Xa38,
 b9 Xb23 + b10 Xb33 = Xa39,
 b9 Xb24 + b10 Xb34 = Xa40,
 b9 Xb25 + b10 Xb35 = Xa41,
 b9 Xb26 + b10 Xb36 = Xa42 ,
 b9 Xb27 + b10 Xb37 = Xa43
 b9 Xb28 + b10 Xb38 = Xa44
 b9 Xb29 + b10 Xb39 = Xa45

b11 Xb11 + b12 Xb31 = Xa46,
 b11 Xb12 + b12 Xb32 = Xa47,
 b11 Xb13 + b12 Xb33 = Xa48,
 b11 Xb14 + b12 Xb34 = Xa49,
 b11 Xb15 + b12 Xb35 = Xa50,
 b11 Xb16 + b12 Xb36 = Xa51 ,
 b11 Xb17 + b12 Xb37 = Xa52
 b11 Xb18 + b12 Xb38 = Xa53
 b11 Xb19 + b12 Xb39 = Xa54 -

b13 Xb11 + b14 Xb31 = Xa55,
 b13 Xb12 + b14 Xb32 = Xa56,
 b13 Xb13 + b14 Xb33 = Xa57,
 b13 Xb14 + b14 Xb34 = Xa58,
 b13 Xb15 + b14 Xb35 = Xa59,
 b13 Xb16 + b14 Xb36 = Xa60 ,
 b13 Xb17 + b14 Xb37 = Xa61
 b13 Xb18 + b14 Xb38 = Xa62
 b13 Xb19 + b14 Xb39 = Xa63

b15 Xb11 + b16 Xb31 = Xa64,
 b15 Xb12 + b16 Xb32 = Xa65,
 b15 Xb13 + b16 Xb33 = Xa66,
 b15 Xb14 + b16 Xb34 = Xa67,
 b15 Xb15 + b16 Xb35 = Xa68,
 b15 Xb16 + b16 Xb36 = Xa69 ,
 b15 Xb17 + b16 Xb37 = Xa70
 b15 Xb18 + b16 Xb38 = Xa71
 b15 Xb19 + b16 Xb39 = Xa72

b17 Xb11 + b18 Xb31 = Xa73,
 b17 Xb12 + b18 Xb32 = Xa74,
 b17 Xb13 + b18 Xb33 = Xa75,
 b17 Xb14 + b18 Xb34 = Xa76,
 b17 Xb15 + b18 Xb35 = Xa77,
 b17 Xb16 + b18 Xb36 = Xa78 ,
 b17 Xb17 + b18 Xb37 = Xa79
 b17 Xb18 + b18 Xb38 = Xa80
 b17 Xb19 + b18 Xb39 = Xa81

B2 u =

Xa1 X10 + Xa2 X11 + Xa3 X12 + Xa4 X13 + Xa5 X14 + Xa6 X15 + Xa7 X16 + Xa8 X17 + Xa9 X18
 Xa10 X10 + Xa11 X11 + Xa12 X12 + Xa13 X13 + Xa14 X14 + Xa15 X15 + Xa16 X16 + Xa17 X17 + Xa18 X18
 Xa19 X10 + Xa20 X11 + Xa21 X12 + Xa22 X13 + Xa23 X14 + Xa24 X15 + Xa25 X16 + Xa26 X17 + Xa27 X18
 Xa28 X10 + Xa29 X11 + Xa30 X12 + Xa31 X13 + Xa32 X14 + Xa33 X15 + Xa34 X16 + Xa35 X17 + Xa36 X18
 Xa37 X10 + Xa38 X11 + Xa39 X12 + Xa40 X13 + Xa41 X14 + Xa42 X15 + Xa43 X16 + Xa44 X17 + Xa45 X18
 Xa46 X10 + Xa47 X11 + Xa48 X12 + Xa49 X13 + Xa50 X14 + Xa51 X15 + Xa52 X16 + Xa53 X17 + Xa54 X18
 Xa55 X10 + Xa56 X11 + Xa57 X12 + Xa58 X13 + Xa59 X14 + Xa60 X15 + Xa61 X16 + Xa62 X17 + Xa63 X18
 Xa64 X10 + Xa65 X11 + Xa66 X12 + Xa67 X13 + Xa68 X14 + Xa69 X15 + Xa70 X16 + Xa71 X17 + Xa72 X18
 Xa73 X10 + Xa74 X11 + Xa75 X12 + Xa76 X13 + Xa77 X14 + Xa78 X15 + Xa79 X16 + Xa80 X17 + Xa81 X18

***Observe 9 states ---

C2t(y - C2 X(10-18*))=

C2 = [1 0 0 0 0 0 0 0 0]	y1 -	1 0 0 0 0 0 0 0 0]	x10
0 1 0 0 0 0 0 0 0]	y2 -	0 1 0 0 0 0 0 0 0]	x11
0 0 1 0 0 0 0 0 0]	y3 -	0 0 1 0 0 0 0 0 0]	x12
0 0 0 1 0 0 0 0 0]	y4 -	0 0 0 1 0 0 0 0 0]	x13
0 0 0 1 0 0 0 0 0]	y5 -	0 0 0 1 0 0 0 0 0]	x14
0 0 0 0 1 0 0 0 0]	y6 -	0 0 0 0 1 0 0 0 0]	x15
0 0 0 0 0 1 0 0 0]	y7 -	0 0 0 0 0 1 0 0 0]	x16
0 0 0 0 0 0 1 0 0]	y8 -	0 0 0 0 0 0 1 0 0]	x17
0 0 0 0 0 0 0 1 0]	y9 -	0 0 0 0 0 0 0 1 0]	x18

C2 = [1 0 0 0 0 0 0 0 0]	y1 - x10	= y1 - x10
0 1 0 0 0 0 0 0 0]	y2 - x11	y2 - x11
0 0 1 0 0 0 0 0 0]	y3 - x12	y3 - x12
0 0 0 1 0 0 0 0 0]	y4 - x13	y4 - x13
0 0 0 1 0 0 0 0 0]	y5 - x14	y5 - x14
0 0 0 0 1 0 0 0 0]	y6 - x15	y6 - x15
0 0 0 0 0 1 0 0 0]	y7 - x16	y7 - x16
0 0 0 0 0 0 1 0 0]	y8 - x17	y8 - x17
0 0 0 0 0 0 0 1 0]	y9 - x18	y9 - x18

Y(9,9) C2T(y - C2 X(10-18*))

Y11	Y12	Y13	Y14	Y15	Y16	Y17	Y18	Y19	y1 - x10
Y12	Y22	Y23	Y24	Y25	Y26	Y27	Y28	Y29	y2 - x11
Y13	Y23	Y33	Y34	Y35	Y36	Y37	Y38	Y39	y3 - x12
= Y14	Y24	Y34	Y44	Y45	Y46	Y47	Y48	Y49	y4 - x13
Y15	Y25	Y35	Y45	Y55	Y56	Y57	Y58	Y59	y5 - x14
Y16	Y26	Y36	Y46	Y56	Y66	Y67	Y68	Y69	y6 - x15
Y17	Y27	Y37	Y47	Y57	Y67	Y77	Y78	Y79	y7 - x16
Y18	Y28	Y38	Y48	Y58	Y68	Y78	Y88	Y89	y8 - x17
Y19	Y29	Y39	Y49	Y59	Y69	Y79	Y89	Y99	y9 - x18

$$\begin{aligned}
 &= \\
 &Y11(y1 - x10) + Y12(y2 - x11) + Y13(y3 - x12) + Y14(y4 - x13) + Y15(y5 - x14) + Y16(y6 - x15) + Y17(y7 - x16) + Y18(y8 - x17) \\
 &Y12(y1 - x10) + Y22(y2 - x11) + Y23(y3 - x12) + Y24(y4 - x13) + Y25(y5 - x14) + Y26(y6 - x15) + Y27(y7 - x16) + Y28(y8 - x17) \\
 &Y13(y1 - x10) + Y23(y2 - x11) + Y33(y3 - x12) + Y34(y4 - x13) + Y35(y5 - x14) + Y36(y6 - x15) + Y37(y7 - x16) + Y38(y8 - x17) \\
 &Y14(y1 - x10) + Y24(y2 - x11) + Y34(y3 - x12) + Y44(y4 - x13) + Y45(y5 - x14) + Y46(y6 - x15) + Y47(y7 - x16) + Y48(y8 - x17) \\
 &Y15(y1 - x10) + Y25(y2 - x11) + Y35(y3 - x12) + Y45(y4 - x13) + Y55(y5 - x14) + Y56(y6 - x15) + Y57(y7 - x16) + Y58(y8 - x17) \\
 &Y16(y1 - x10) + Y26(y2 - x11) + Y36(y3 - x12) + Y46(y4 - x13) + Y56(y5 - x14) + Y66(y6 - x15) + Y67(y7 - x16) + Y68(y8 - x17) \\
 &Y17(y1 - x10) + Y27(y2 - x11) + Y37(y3 - x12) + Y47(y4 - x13) + Y57(y5 - x14) + Y67(y6 - x15) + Y77(y7 - x16) + Y78(y8 - x17) \\
 &Y18(y1 - x10) + Y28(y2 - x11) + Y38(y3 - x12) + Y48(y4 - x13) + Y58(y5 - x14) + Y68(y6 - x15) + Y78(y7 - x16) + Y88(y8 - x17) \\
 &Y19(y1 - x10) + Y29(y2 - x11) + Y39(y3 - x12) + Y49(y4 - x13) + Y59(y5 - x14) + Y69(y6 - x15) + Y79(y7 - x16) + Y89(y8 - x17)
 \end{aligned}$$

= -	Y11 x10 + Y12 x11 + Y13 x12 + Y14 x13 + Y15 x14 + Y16 x15 + Y17 x16 + Y18 x17 + Y19 x18	+Y19 (y9 - x18)						
	Y12 x10 + Y22 x11 + Y23 x12 + Y24 x13 + Y25 x14 + Y26 x15 + Y27 x16 + Y28 x17 + Y29 x18	+Y49 (y9 - x18)						
	Y13 x10 + Y23 x11 + Y33 x12 + Y34 x13 + Y35 x14 + Y36 x15 + Y37 x16 + Y38 x17 + Y39 x18	+Y59 (y9 - x18)						
	Y14 x10 + Y24 x11 + Y34 x12 + Y44 x13 + Y45 x14 + Y46 x15 + Y47 x16 + Y48 x17 + Y49 x18	+Y69 (y9 - x18)						
	Y15 x10 + Y25 x11 + Y35 x12 + Y45 x13 + Y55 x14 + Y56 x15 + Y57 x16 + Y58 x17 + Y59 x18	+Y79 (y9 - x18)						
	Y16 x10 + Y26 x11 + Y36 x12 + Y46 x13 + Y56 x14 + Y66 x15 + Y67 x16 + Y68 x17 + Y69 x18	+Y89 (y9 - x18)						
	Y17 x10 + Y27 x11 + Y37 x12 + Y47 x13 + Y57 x14 + Y67 x15 + Y77 x16 + Y78 x17 + Y79 x18	+Y99 (y9 - x18)						
	Y18 x10 + Y28 x11 + Y38 x12 + Y48 x13 + Y58 x14 + Y68 x15 + Y78 x16 + Y88 x17 + Y89 x18							
	Y19 x10 + Y29 x11 + Y39 x12 + Y49 x13 + Y59 x14 + Y69 x15 + Y79 x16 + Y89 x17 + Y99 x18							
Y11 y1	+Y12 y2	+Y13 y3	+Y14 y4	+Y15 y5	+Y16 y6	+Y17 y7	+Y18 y8	+Y19 y9
Y12 y1	+Y22 y2	+Y23 y3	+Y24 y4	+Y25 y5	+Y26 y6	+Y27 y7	+Y28 y8	+Y29 y9
Y13 y1	+Y23 y2	+Y33 y3	+Y34 y4	+Y35 y5	+Y36 y6	+Y37 y7	+Y38 y8	+Y39 y9
Y14 y1	+Y24 y2	+Y34 y3	+Y44 y4	+Y45 y5	+Y46 y6	+Y47 y7	+Y48 y8	+Y49 y9
Y15 y1	+Y25 y2	+Y35 y3	+Y45 y4	+Y55 y5	+Y56 y6	+Y57 y7	+Y58 y8	+Y59 y9
Y16 y1	+Y26 y2	+Y36 y3	+Y46 y4	+Y56 y5	+Y66 y6	+Y67 y7	+Y68 y8	+Y69 y9
Y17 y1	+Y27 y2	+Y37 y3	+Y47 y4	+Y57 y5	+Y67 y6	+Y77 y7	+Y78 y8	+Y79 y9
Y18 y1	+Y28 y2	+Y38 y3	+Y48 y4	+Y58 y5	+Y68 y6	+Y78 y7	+Y88 y8	+Y89 y9
Y19 y1	+Y29 y2	+Y39 y3	+Y49 y4	+Y59 y5	+Y69 y6	+Y79 y7	+Y89 y8	+Y99 y9

%-----

Ob1 = (a11 - Xa1 - Y(1,1))	Ob28= (0 - Xa28 - Y(1,4))	Ob55= (0 - Xa55 - Y(1,7))
Ob2 = (a12 - Xa2 - Y(1,2))	Ob29= (0 - Xa29 - Y(2,4))	Ob56= (0 - Xa56 - Y(2,7))
Ob3 = (a13 - Xa3 - Y(1,3))	Ob30= (a43 - Xa30 - Y(3,4))	Ob57= (0 - Xa57 - Y(3,7))
Ob4 = (a14 - Xa4 - Y(1,4))	Ob31= (0 - Xa31 - Y(4,4))	Ob58= (a74 - Xa58 - Y(4,7))
Ob5 = (a15 - Xa5 - Y(1,5))	Ob32= (a45 - Xa32 - Y(4,5))	Ob59= (0 - Xa59 - Y(5,7))
Ob6 = (a16 - Xa6 - Y(1,6))	Ob33= (0 - Xa33 - Y(4,6))	Ob60= (a76 - Xa60 - Y(6,7))
Ob7 = (a17 - Xa7 - Y(1,7))	Ob34= (a47 - Xa34 - Y(4,7))	Ob61= (0 - Xa61 - Y(7,7))
Ob8 = (a18 - Xa8 - Y(1,8))	Ob35= (0 - Xa35 - Y(4,8))	Ob62= (a78 - Xa62 - Y(7,8))
Ob9 = (a19 - Xa9 - Y(1,9))	Ob36= (0 - Xa36 - Y(4,9))	Ob63= (0 - Xa63 - Y(7,9))

%-----

Ob1s = -Y(1,1)	Ob16s = -Y(1,4)	Ob31s = -Y(1,7)
Ob2s = -Y(1,2)	Ob17s = -Y(2,4)	Ob32s = -Y(2,7)
Ob3s = -Y(1,3)	Ob18s = -Y(3,4)	Ob33s = -Y(3,7)
Ob4s = -Y(1,4)	Ob19s = -Y(4,4)	Ob34s = -Y(4,7)
Ob5s = -Y(1,5)	Ob20s = -Y(4,5)	Ob35s = -Y(5,7)
Ob1ss =- Y(1,6)	Ob16ss =- Y(4,6)	Ob31ss =- Y(6,7)
Ob2ss =- Y(1,7)	Ob17ss =- Y(4,7)	Ob32ss =- Y(7,7)
Ob3ss =- Y(1,8)	Ob18ss =- Y(4,8)	Ob33ss =- Y(7,8)
Ob4ss =- Y(1,9)	Ob19ss =- Y(4,9)	Ob34ss =- Y(7,9)

%-----

Ob10= (a21 - Xa10 - Y(1,2))	Ob37= (0 - Xa37 - Y(1,5))	Ob64= (0 - Xa64 - Y(1,8))
Ob11= (0 - Xa11 - Y(2,2))	Ob38= (0 - Xa38 - Y(2,5))	Ob65= (0 - Xa65 - Y(2,8))
Ob12= (a23 - Xa12 - Y(2,3))	Ob39= (0 - Xa39 - Y(3,5))	Ob66= (a83 - Xa66 - Y(3,8))
Ob13= (0 - Xa13 - Y(2,4))	Ob40= (a54 - Xa40 - Y(4,5))	Ob67= (0 - Xa67 - Y(4,8))
Ob14= (0 - Xa14 - Y(2,5))	Ob41= (0 - Xa41 - Y(5,5))	Ob68= (0 - Xa68 - Y(5,8))
Ob15= (0 - Xa15 - Y(2,6))	Ob42= (a56 - Xa42 - Y(5,6))	Ob69= (0 - Xa69 - Y(6,8))
Ob16= (0 - Xa16 - Y(2,7))	Ob43= (0 - Xa43 - Y(5,7))	Ob70= (a87 - Xa70 - Y(7,8))
Ob17= (0 - Xa17 - Y(2,8))	Ob44= (0 - Xa44 - Y(5,8))	Ob71= (0 - Xa71 - Y(8,8))
Ob18= (a29 - Xa18 - Y(2,9))	Ob45= (0 - Xa45 - Y(5,9))	Ob72= (a89 - Xa72 - Y(8,9))

%-----

Ob6s = -Y(1,2)	Ob21s = -Y(1,5)	Ob36s = -Y(1,8)
Ob7s = -Y(2,2)	Ob22s = -Y(2,5)	Ob37s = -Y(2,8)
Ob8s = -Y(2,3)	Ob23s = -Y(3,5)	Ob38s = -Y(3,8)
Ob9s = -Y(2,4)	Ob24s = -Y(4,5)	Ob39s = -Y(4,8)
Ob10s =- Y(2,5)	Ob25s = -Y(5,5)	Ob40s = -Y(5,8)
Ob6ss =- Y(2,6)	Ob21ss =- Y(5,6)	Ob36ss =- Y(6,8)
Ob7ss =- Y(2,7)	Ob22ss =- Y(5,7)	Ob37ss =- Y(7,8)
Ob8ss =- Y(2,8)	Ob23ss =- Y(5,8)	Ob38ss =- Y(8,8)
Ob9ss =- Y(2,9)	Ob24ss =- Y(5,9)	Ob39ss =- Y(8,9)

%-----

Ob19= (0 - Xa19 - Y(1,3))	Ob46= (0 - Xa46 - Y(1,6))	Ob73= (a91 - Xa73 - Y(1,9))
Ob20= (a32 - Xa20 - Y(2,3))	Ob47= (0 - Xa47 - Y(2,6))	Ob74= (a92 - Xa74 - Y(2,9))
Ob21= (0 - Xa21 - Y(3,3))	Ob48= (0 - Xa48 - Y(3,6))	Ob75= (a93 - Xa75 - Y(3,9))
Ob22= (a34 - Xa22 - Y(3,4))	Ob49= (0 - Xa49 - Y(4,6))	Ob76= (a94 - Xa76 - Y(4,9))
Ob23= (0 - Xa23 - Y(3,5))	Ob50= (a65 - Xa50 - Y(5,6))	Ob77= (a95 - Xa77 - Y(5,9))
Ob24= (0 - Xa24 - Y(3,6))	Ob51= (0 - Xa51 - Y(6,6))	Ob78= (a96 - Xa78 - Y(6,9))
Ob25= (0 - Xa25 - Y(3,7))	Ob52= (a67 - Xa52 - Y(6,7))	Ob79= (a97 - Xa79 - Y(7,9))
Ob26= (a38 - Xa26 - Y(3,8))	Ob53= (0 - Xa53 - Y(6,8))	Ob80= (a98 - Xa80 - Y(8,9))
Ob27= (0 - Xa27 - Y(3,9))	Ob54= (0 - Xa54 - Y(6,9))	Ob81= (a99 - Xa81 - Y(9,9))

%-----

Ob11s = -Y(1,3)	Ob26s = -Y(1,6)	Ob41s = -Y(1,9)
Ob12s = -Y(2,3)	Ob27s = -Y(2,6)	Ob42s = -Y(2,9)
Ob13s = -Y(3,3)	Ob28s = -Y(3,6)	Ob43s = -Y(3,9)
Ob14s = -Y(3,4)	Ob29s = -Y(4,6)	Ob44s = -Y(4,9)
Ob15s = -Y(3,5)	Ob30s = -Y(5,6)	Ob45s = -Y(5,9)
Ob11ss =- Y(3,6)	Ob26ss =- Y(6,6)	Ob41ss =- Y(6,9)
Ob12ss =- Y(3,7)	Ob27ss =- Y(6,7)	Ob42ss =- Y(7,9)
Ob13ss =- Y(3,8)	Ob28ss =- Y(6,8)	Ob43ss =- Y(8,9)
Ob14ss =- Y(3,9)	Ob29ss =- Y(6,9)	Ob44ss =- Y(9,9)

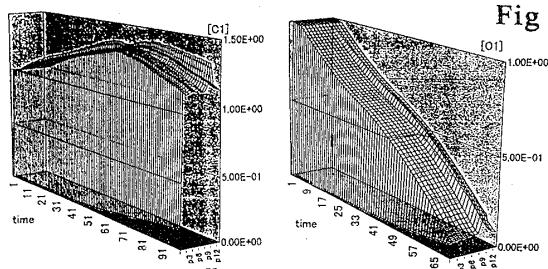
%-----

$\dot{x}(1) = a_{11}x(1) + a_{12}x(2) + a_{13}x(3) + a_{14}x(4) + a_{15}x(5) + a_{16}x(6) + a_{17}x(7) + a_{18}x(8) + a_{19}x(9)$
 $+ Xa1*x(10) + Xa2*x(11) + Xa3*x(12) + Xa4*x(13) + Xa5*x(14) + Xa6*x(15) + Xa7*x(16) + Xa8*x(17) + Xa9*x(18)$
 $\dot{x}(2) = a_{21}x(1) + a_{23}x(3) + a_{29}x(9)$
 $+ Xa10*x(10) + Xa11*x(11) + Xa12*x(12) + Xa13*x(13) + Xa14*x(14) + Xa15*x(15) + Xa16*x(16) + Xa17*x(17) + Xa18*x(18)$
 $\dot{x}(3) = a_{32}x(2) + a_{34}x(4) + a_{38}x(8)$
 $+ Xa19*x(10) + Xa20*x(11) + Xa21*x(12) + Xa22*x(13) + Xa23*x(14) + Xa24*x(15) + Xa25*x(16) + Xa26*x(17) + Xa27*x(18)$
 $\dot{x}(4) = a_{43}x(3) + a_{45}x(5) + a_{47}x(7)$
 $+ Xa28*x(10) + Xa29*x(11) + Xa30*x(12) + Xa31*x(13) + Xa32*x(14) + Xa33*x(15) + Xa34*x(16) + Xa35*x(17) + Xa36*x(18)$
 $\dot{x}(5) = a_{54}x(4) + a_{56}x(6)$
 $+ Xa37*x(10) + Xa38*x(11) + Xa39*x(12) + Xa40*x(13) + Xa41*x(14) + Xa42*x(15) + Xa43*x(16) + Xa44*x(17) + Xa45*x(18)$
 $\dot{x}(6) = a_{65}x(5) + a_{67}x(7)$
 $+ Xa46*x(10) + Xa47*x(11) + Xa48*x(12) + Xa49*x(13) + Xa50*x(14) + Xa51*x(15) + Xa52*x(16) + Xa53*x(17) + Xa54*x(18)$
 $\dot{x}(7) = a_{74}x(4) + a_{76}x(6) + a_{78}x(8)$
 $+ Xa55*x(10) + Xa56*x(11) + Xa57*x(12) + Xa58*x(13) + Xa59*x(14) + Xa60*x(15) + Xa61*x(16) + Xa62*x(17) + Xa63*x(18)$
 $\dot{x}(8) = a_{83}x(3) + a_{87}x(7) + a_{89}x(9)$
 $+ Xa64*x(10) + Xa65*x(11) + Xa66*x(12) + Xa67*x(13) + Xa68*x(14) + Xa69*x(15) + Xa70*x(16) + Xa71*x(17) + Xa72*x(18)$
 $\dot{x}(9) = a_{91}x(1) + a_{92}x(2) + a_{93}x(3) + a_{94}x(4) + a_{95}x(5) + a_{96}x(6) + a_{97}x(7) + a_{98}x(8) + a_{99}x(9)$
 $+ Xa73*x(10) + Xa74*x(11) + Xa75*x(12) + Xa76*x(13) + Xa77*x(14) + Xa78*x(15) + Xa79*x(16) + Xa80*x(17) + Xa81*x(18)$
 $\dot{x}(10) = Ob1*x(10) + Ob2*x(11) + Ob3*x(12) + Ob4*x(13) + Ob5*x(14) + Ob6*x(15) + Ob7*x(16) + Ob8*x(17) + Ob9*x(18)$
 $+ Ob1s*x(1) + Ob2s*x(2) + Ob3s*x(3) + Ob4s*x(4) + Ob5s*x(5) + Ob1ss*x(6) + Ob2ss*x(7) + Ob3ss*x(8) + Ob4ss*x(9)$
 $\dot{x}(11) = Ob10*x(10) + Ob11*x(11) + Ob12*x(12) + Ob13*x(13) + Ob14*x(14) + Ob15*x(15) + Ob16*x(16) + Ob17*x(17) + Ob18*x(18)$
 $+ Ob6s*x(1) + Ob7s*x(2) + Ob8s*x(3) + Ob9s*x(4) + Ob10s*x(5) + Ob16ss*x(6) + Ob17ss*x(7) + Ob18ss*x(8) + Ob19ss*x(9)$
 $\dot{x}(12) = Ob19*x(10) + Ob20*x(11) + Ob21*x(12) + Ob22*x(13) + Ob23*x(14) + Ob24*x(15) + Ob25*x(16) + Ob26*x(17)$
 $+ Ob27*x(18) + Ob11s*x(1) + Ob12s*x(2) + Ob13s*x(3) + Ob14s*x(4) + Ob15s*x(5) + Ob11ss*x(6) + Ob12ss*x(7)$
 $+ Ob13ss*x(8) + Ob14ss*x(9)$
 $\dot{x}(13) = Ob28*x(10) + Ob29*x(11) + Ob30*x(12) + Ob31*x(13) + Ob32*x(14) + Ob33*x(15) + Ob34*x(16) + Ob35*x(17) + Ob36*x(18)$
 $+ Ob16s*x(1) + Ob17s*x(2) + Ob18s*x(3) + Ob19s*x(4) + Ob20s*x(5) + Ob16ss*x(6) + Ob17ss*x(7) + Ob18ss*x(8) + Ob19ss*x(9)$
 $\dot{x}(14) = Ob37*x(10) + Ob38*x(11) + Ob39*x(12) + Ob40*x(13) + Ob41*x(14) + Ob42*x(15) + Ob43*x(16)$
 $+ Ob44*x(17) + Ob45*x(18) + Ob21s*x(1) + Ob22s*x(2) + Ob23s*x(3) + Ob24s*x(4) + Ob25s*x(5) + Ob21ss*x(6)$
 $+ Ob22ss*x(7) + Ob23ss*x(8) + Ob24ss*x(9)$
 $\dot{x}(15) = Ob46*x(10) + Ob47*x(11) + Ob48*x(12) + Ob49*x(13) + Ob50*x(14) + Ob51*x(15) + Ob52*x(16) + Ob53*x(17) + Ob54*x(18)$
 $+ Ob26s*x(1) + Ob27s*x(2) + Ob28s*x(3) + Ob29s*x(4) + Ob30s*x(5) + Ob26ss*x(6) + Ob27ss*x(7) + Ob28ss*x(8) + Ob29ss*x(9)$
 $\dot{x}(16) = Ob55*x(10) + Ob56*x(11) + Ob57*x(12) + Ob58*x(13) + Ob59*x(14) + Ob60*x(15) + Ob61*x(16) + Ob62*x(17) + Ob63*x(18)$
 $+ Ob31s*x(1) + Ob32s*x(2) + Ob33s*x(3) + Ob34s*x(4) + Ob35s*x(5) + Ob31ss*x(6) + Ob32ss*x(7) + Ob33ss*x(8) + Ob34ss*x(9)$
 $\dot{x}(17) = Ob64*x(10) + Ob65*x(11) + Ob66*x(12) + Ob67*x(13) + Ob68*x(14) + Ob69*x(15) + Ob70*x(16) + Ob71*x(17) + Ob72*x(18)$
 $+ Ob36s*x(1) + Ob37s*x(2) + Ob38s*x(3) + Ob39s*x(4) + Ob40s*x(5) + Ob36ss*x(6) + Ob37ss*x(7) + Ob38ss*x(8) + Ob39ss*x(9)$
 $\dot{x}(18) = Ob73*x(10) + Ob74*x(11) + Ob75*x(12) + Ob76*x(13) + Ob77*x(14) + Ob78*x(15) + Ob79*x(16) + Ob80*x(17) + Ob81*x(18)$
 $+ Ob41s*x(1) + Ob42s*x(2) + Ob43s*x(3) + Ob44s*x(4) + Ob45s*x(5) + Ob41ss*x(6) + Ob42ss*x(7) + Ob43ss*x(8) + Ob44ss*x(9)$

To close the loop, we set the negative feed back as

$$\begin{aligned}
y_1 &= -x_1, \\
y_2 &= -x_2, \\
y_3 &= -x_3, \\
y_4 &= -x_4, \\
y_5 &= -x_5, \\
y_6 &= -x_6, \\
y_7 &= -x_7, \\
y_8 &= -x_8, \\
y_9 &= -x_9,
\end{aligned}$$

We can obtain the coefficients Ob_n and Ob_{nss}



2. Results.

Fig 5 shows the temporal changes in $[C1]$ and $[O1]$ with changes in weighting coefficients for the control inputs un . Significant changes can be observed at particular pn . The present evaluation when extended will be available for predicting the noise filtering function of biomembranes.

3. Reference

- Matkes.T.N and Jones.W. J.Gen. Phys. vol 99. pp 367. 1992.