

Linear Systems Analysis of Systolic Coronary Circulation.

H, Hirayama., N, Kitagawa., Y, Okita and T, Kazui.

Department of Public Health Asahikawa medical college
The Graduate School of Shizuoka university
The First Department of Surgery Hamamatsu medical college.

Linear system analysis was applied for the coronary circulation system. The system was expressed by an equivalent electrical circuit. It is consisted of the arterial and venous sites each of which is separated to the epicardial and the endocardial regions. The mechanical properties of the vessels were expressed by resistance and capacitance which values were adopted from the reported animal experiments. The system was expressed by 4 linear differential equations. The control inputs to drive the blood during the systolic phase were set by the active elastance of cardiac muscles. At the physiological resistance and capacitance, the system was stable and controllable. Expressing the coronary arterial sclerosis by reducing the capacitance and arterial stenosis by increasing the resistance, we can evaluate the pathophysiological changes in coronary circulation.

Coronary circulation, Equivalent electrical circuit, Epicardium, Endocardium, Resistance, Capacitance

冠循環に対する線形システム特性

平山博史, 北川敬之, *沖田善光, **数井暉久

旭川市西神楽4-5 旭川医科大学 公衆衛生学講座
(電話0166-65-2111、内2411) E mail hirayama@asahikawa-med.ac.jp

* 静岡大学大学院電子科学研究施設

** 浜松医科大学外科学第一講座

冠循環のシステム特性を解析した。冠循環を電氣的等価回路モデルで表現した。モデルは動脈側、静脈側から構成され、それぞれ心外膜近傍、心内膜近傍に分離した。血管特性は抵抗とキャパシタンスで表現した。冠血管の各部位における抵抗値とキャパシタンスの値とは動物実験で報告されている結果を採用した。系は4個の線形微分方程式で記述された。制御入力としては、収縮期心筋能動弾性を想定し、これが心外膜近傍および心内膜近傍の心筋に作用して心筋内冠血管を圧迫することで収縮期の心筋内冠血管内の逆流がおきるとした。生理的血管抵抗、キャパシタンスでは系は安定であった。また制御であった。本研究をより複雑にすることで冠動脈硬化を血管キャパシタンスの低下、また冠血管狭窄を血流抵抗の上昇で表現することで系の動特性の変化を定量的に評価することが可能である。

冠循環. 電氣的等価回路モデル. 心外膜近傍. 心内膜近傍. 抵抗. キャパシタンス

1. Introduction.

A lot of experimental studies have performed (Kajiya 1990) to characterize coronary circulation. By associating those findings and to understand intuitively, several models (Downey 1975, Spaan 1981, Krams 1989) have been proposed. In the present work, we apply linear systems analysis to evaluate an entire systemic properties of the systolic coronary circulation.

2. Mathematical method.

2-1. Construction of equivalent electrical model of coronary circulation.

Fig 1 shows the equivalent electrical circuit of the coronary circulation. Coronary vessel properties in each compartment are comprised of blood flow resistance R_n and compliance C_n . The left part describes the epicardial surface arterial system. Exogenous input for the coronary circulation system is supplied by aortic pressure $P_a(t)$. The middle part illustrates circulation within the myocardium. It is comprised of the region near to the epicardium (upper portion) and the region near to the endocardium (lower portion). The blood flow in each region of it is controlled by the pressures produced by the active elastance of cardiac muscle (at near the epicardium : $P_{epi}(t)$ and at near the endocardium : $P_{end}(t)$) and the passive pressures ($P_2(t)$, $P_3(t)$). The left half of the middle part expresses the intramyocardial arterial system and right one the intramyocardial venous system. The right part expresses the epicardial surface venous system. Atrial pressure P_e was set to be constant. Derivation of mathematical equations are shown in Appendix 1. The resistance (mmHgsec/ml) are $R_1 = 1$; $R_2 = 1$; $R_3 = 50$; $R_4 = 100$; $R_5 = 25$; $R_6 = 75$; $R_7 = 0.5$; $R_8 = 0.5$ and capacitance (ml/mmHg) are

$C_1 = 0.1$; $C_2 = 0.05$; $C_3 = 0.01$; $C_4 = 0.2$;

Eigen values of the system were examined by the characteristic equation of the system.

The singular values of the system $C(j\omega I - A)^{-1}B$ are shown in Fig 3. The left column is obtained by setting all the control inputs unity while the right column is obtained by setting b_4, b_5, b_{10}, b_{11} et as exact form that were

Table 1. Definition of the Electrical Circuit

- $P_a(t)$: aortic pressure driving the coronary circulation.
- $P_1(t)$: epicardial surface arterial pressure degraded by arterial resistance R_1 at the near to aorta.
- F_1 : coronary arterial blood flow rate from aorta.
- F_2 : coronary arterial flow rate at the epicardium immediately before the artery runs into myocardium.
- R_1 : fluid resistance for blood flow at the epicardium near to aorta,
- C_1 : arterial compliance at the epicardium near to aorta.
- R_2 : epicardial arterial resistance at the epicardium
- F_3 : arterial flow at near the epicardium region .
- F_5 : venous flow at near the epicardium region
- R_3 : arterial resistance for $F_3(t)$ at near the epicardium region.
- R_5 : venous resistance for $F_5(t)$ at near the epicardium region.
- C_2 : arterial compliance at near the epicardium region.
- $P_2(t)$: passive extra vascular pressure on $C_2(t)$ at the epi cardium.
- $P_{epi}(t)$: active pressure generated by active contraction of cardiac muscle at near the epicardial region .
- F_4 : arterial flow at near the endocardium region.
- F_6 : venous flow at near the endocardium region.
- R_4 : arterial resistance for $F_4(t)$ at near the endocardium region.
- R_6 : venous resistance for $F_6(t)$ at near the endocardium region.
- C_3 : arterial compliance at near the endocardium region.
- $P_3(t)$: passive extra vascular pressure on $C_3(t)$ at the endocardium
- $P_{end}(t)$: active pressure generated by active contraction of cardiac muscle fiber at near the endocardium region .
- P_e : pressure at right atrium,
- F_8 : the extra myocardial venous flow before the venous flows
- R_8 : resistance for venous flow $F_8(t)$.
- C_4 : compliance for the epicardial vein.
- F_7 : venous flow in the epicardium.
- R_7 : resistance for $F_7(t)$.
- $P_4(t)$: pressure on vein at the epicardium.

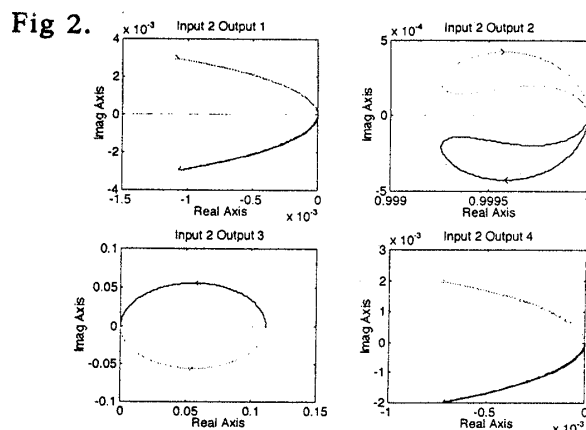


Fig 1. An equivalent electrical circuit for coronary circulation.

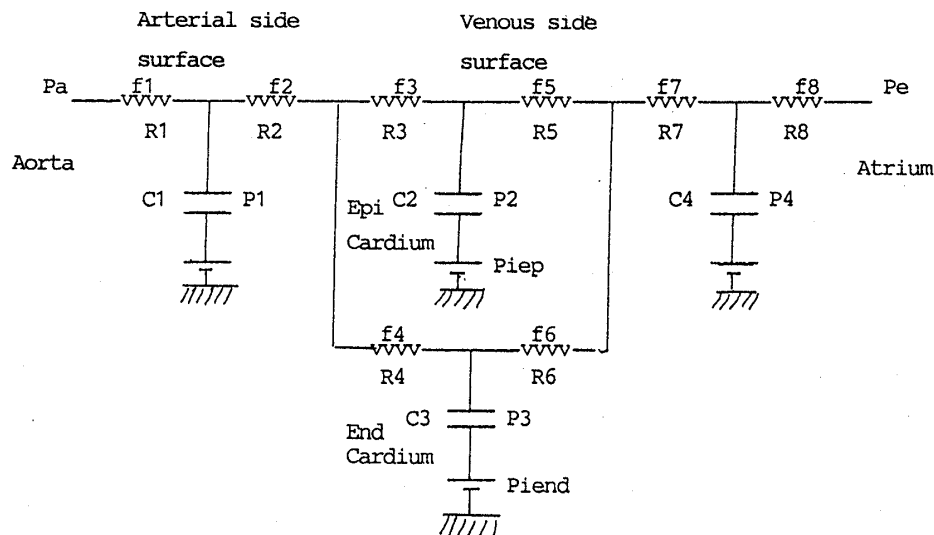
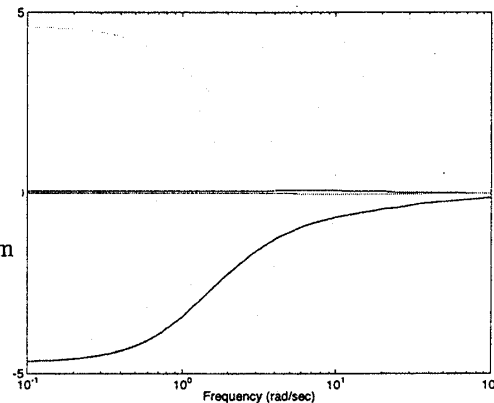
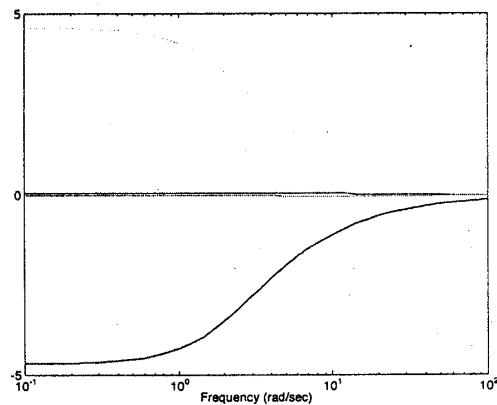
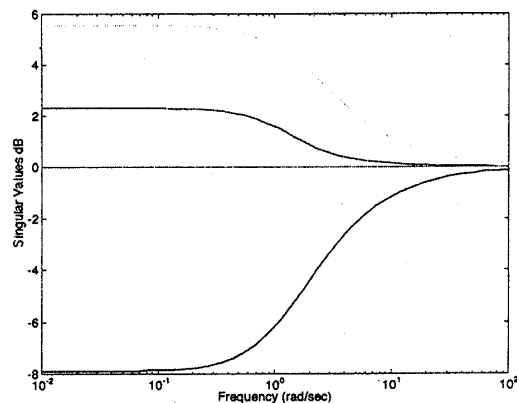
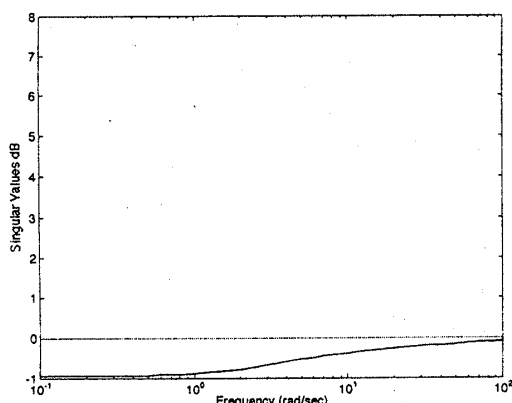
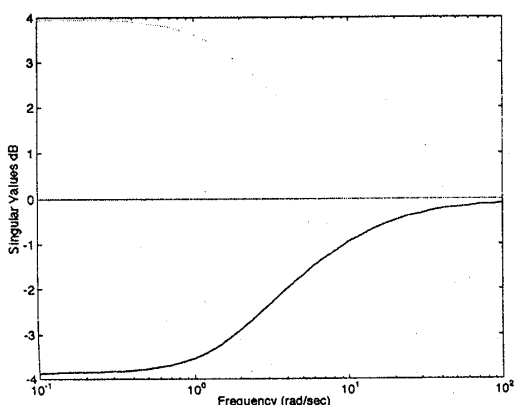
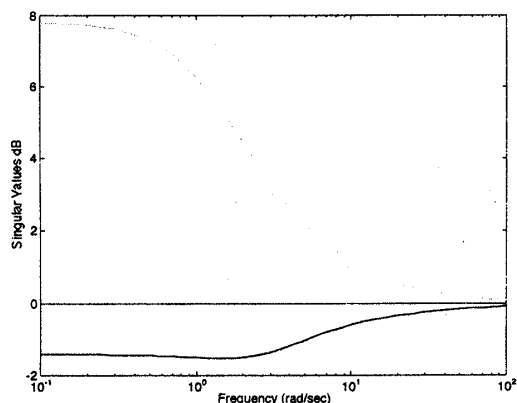


Fig 3.



Singular Values
Strong negative
feed back on
the control input
of the epicardium
(Piep)

Singular Values
Strong negative
feed back on
the control input
of the endocardium
(Pend)

given in the APPENDIX 1 for the coefficients of the control inputs P_{ei} (epicardial active pressure) and P_{end} (endocardial one).

3. Results and Discussion. The system was judged to be stable and controllable. All the real parts of the eigen values were negative. The nyquist loops escaped the critical point $-1 + 0j$. The singular values converged to 0 as the frequency (rad/sec) increased. As the control inputs have realized to be physiological ones (right column), all the singular values decreased. The magnitude

A mathematical method for computing the optimized present system characterized by minimizing the performance function

$$L = \int_0^4 [\sum_{n=1}^4 \alpha_n P_n'(t)^2 + \beta_1 U_0(t)^2 + \beta_2 U_e(t)^2 + \beta_3 U_i(t)^2 + \beta_4 U_n(t)^2] dt$$

is shown in APPENDIX 2.

of the feed back on the control inputs influenced strongly on the singular values.

4. Conclusion.

The coronary circulation may be stable and controllable but an intense comparison to experiments is necessary.

6. References.

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[APPENDIX 1].

The differential equations for the coronary blood flow are

$$\begin{aligned} f_1(t) - f_2(t) &= C_1 \frac{dP_1(t)}{dt} & \text{-----(1)} \\ f_2(t) &= f_3(t) + f_4(t) & \text{-----(2)} \\ f_3(t) - f_5(t) &= C_2 \frac{dP_2(t)}{dt} & \text{-----(3)} \\ f_4(t) - f_6(t) &= C_3 \frac{dP_3(t)}{dt} & \text{-----(4)} \\ f_7(t) &= f_5(t) + f_6(t) & \text{-----(5)} \\ f_7(t) - f_8(t) &= C_4 \frac{dP_4(t)}{dt} & \text{-----(6)} \end{aligned}$$

The equations for the coronary vessel pressures are

$$\begin{aligned} P_0(t) - P_1(t) &= R_1 f_1(t) & \text{-----(7)} \\ P_1(t) - (P_2(t) + \text{Piep}(t)) &= R_2 f_2(t) + R_3 f_3(t) & \text{---(8)} \\ P_1(t) - (P_3(t) + \text{Pied}(t)) &= R_2 f_2(t) + R_4 f_4(t) & \text{---(9)} \\ (P_2(t) + \text{Piep}(t)) - P_4(t) &= R_5 f_5(t) + R_7 f_7(t) & \text{---(10)} \\ (P_3(t) + \text{Pied}(t)) - P_4(t) &= R_6 f_6(t) + R_7 f_7(t) & \text{---(11)} \\ P_4(t) - P_e(t) &= R_8 f_8(t) & \text{---(12)} \end{aligned}$$

To obtain the differential equations for the pressure, we express $f_n(t)$ by $p_n(t)$. From equation (2),(8) and (9), we have equations containing only $f_3(t)$ and $f_4(t)$. From (8) and (9),

$$\begin{aligned} R_2 f_2 + R_3 f_3 &= P_1 - P_2 - \text{Piepi} \\ R_2 f_2 + R_4 f_4 &= P_1 - P_3 - \text{Pied} \end{aligned}$$

Substitute

$$f_2 = f_3 + f_4$$

and rearrange

$$\begin{aligned} (R_2 + R_3) f_3 + R_2 f_4 &= P_1 - P_2 - \text{Piepi} \\ R_2 f_3 + (R_2 + R_4) f_4 &= P_1 - P_3 - \text{Pied} \end{aligned}$$

Here, we set

$$\begin{aligned} a_1 &= R_2 + R_3, \quad a_2 = R_2 \\ a_3 &= R_2, \quad a_4 = R_2 + R_4 \end{aligned}$$

and

$$\begin{aligned} g_1(t) &= P_1(t) - P_2(t) - \text{Piep}(t) \\ g_2(t) &= P_1(t) - P_3(t) - \text{Pied}(t) \end{aligned}$$

Then, we have

$$\begin{aligned} a_1 f_3 + a_2 f_4 &= g_1 \\ a_3 f_3 + a_4 f_4 &= g_2 \end{aligned}$$

Here we set

$$a_5 = a_1 a_4 - a_3 a_2, \quad a_6 = a_4 / a_5, \quad a_7 = -a_2 / a_5$$

We eliminate $f_4(t)$. Then we have

$$\begin{aligned} f_3(t) &= a_6 g_1(t) + a_7 g_2(t) \\ &= (a_6 + a_7) P_1 - a_6 P_2 - a_7 P_3 - a_6 \text{Piepi} - a_7 \text{Pied} & \text{---(13)} \end{aligned}$$

$$\begin{aligned} f_4(t) &= a_9 g_1(t) + a_{10} g_2(t) \\ &= (a_9 + a_{10}) P_1 - a_9 P_2 - a_{10} P_3 - a_9 \text{Piepi} - a_{10} \text{Pied} & \text{---(14)} \end{aligned}$$

from equations (5), (10) and (11), we have

$$\begin{aligned} (R_5 + R_7) f_5 + R_7 f_6 &= P_2 + \text{Piepi} - P_4 \\ R_7 f_5 + (R_6 + R_7) f_6 &= P_3 + \text{Pied} - P_4 \end{aligned}$$

Setting

$$\begin{aligned} a_{11} &= R_5 + R_7, \quad a_{12} = R_7 \\ a_{13} &= R_7, \quad a_{14} = R_6 + R_7 \end{aligned}$$

and

$$\begin{aligned} g_3(t) &= P_2(t) + \text{Piepi}(t) - P_4(t) \\ g_4(t) &= P_3(t) + \text{Pied}(t) - P_4(t) \end{aligned}$$

We have two simultaneous equations

$$\begin{aligned} a_{11} f_5(t) + a_{12} f_6(t) &= g_3(t) \\ a_{13} f_5(t) + a_{14} f_6(t) &= g_4(t) \end{aligned}$$

Putting

$$\begin{aligned} a_{15} &= a_{14} a_{11} - a_{12} a_{13}, \quad a_{16} = a_{14} / a_{15} \\ a_{17} &= -a_{12} / a_{15} \end{aligned}$$

We obtain

$$\begin{aligned} f_5(t) &= a_{16} g_3(t) + a_{17} g_4(t) \\ &= a_{16} P_2 + a_{17} P_3 + a_{16} \text{Piep} + a_{17} \text{Pied} \\ &\quad + P_4 (-a_{16} - a_{17}) & \text{-----(15)} \end{aligned}$$

$$\begin{aligned} f_6(t) &= a_{19} g_3(t) + a_{20} g_4(t) \\ &= a_{19} P_2 + a_{20} P_3 + a_{19} \text{Piep} + a_{20} \text{Pied} \\ &\quad + P_4 (-a_{19} - a_{20}) & \text{-----(16)} \end{aligned}$$

Thus, the differential equations for $P_1(t)$ is from the equations (1) and (2).

$$C_1 P_1'(t) = f_1 - f_3 - f_4$$

Substitute this by the equations (7), (13) and (14)

$$\begin{aligned} C_1 P_1' &= (P_0 - P_1) / R_1 \\ &\quad - (a_6 + a_7) P_1 + a_6 P_2 + a_7 P_3 + a_6 \text{Piep} + a_7 \text{Pied} \\ &\quad - (a_9 + a_{10}) P_1 + a_9 P_2 + a_{10} P_3 + a_9 \text{Piep} + a_{10} \text{Pied} \end{aligned}$$

Putting

$$\begin{aligned} b_0 &= 1 / (R_1 C_1) \\ b_1 &= [-1/R_1 - (a_6 + a_7) - (a_9 + a_{10})] / C_1 \\ b_2 &= (a_6 + a_9) / C_1, \quad b_3 = (a_7 + a_{10}) / C_1 \\ b_4 &= (a_6 + a_9) / C_1, \quad b_5 = b_3 \end{aligned}$$

Then we have

$$\begin{aligned} P_1'(t) &= b_0 P_0(t) + b_1 P_1(t) + b_2 P_2(t) + b_3 P_3(t) \\ &\quad + b_4 \text{Piep}(t) + b_5 \text{Pied}(t) & \text{-----(17)} \end{aligned}$$

The differential equation for $P_2(t)$ is

$$\begin{aligned} C_2 P_2'(t) &= f_3(t) - f_5(t) \\ &= (a_6 + a_7) P_1 - a_6 P_2 - a_7 P_3 - a_6 \text{Piep} - a_7 \text{Pied} \\ &\quad - a_{16} P_2 - a_{17} P_3 + (a_{16} + a_{17}) P_4 \\ &\quad - a_{16} \text{Piep} - a_{17} \text{Pied} \end{aligned}$$

Putting

$$\begin{aligned} b_6 &= (a_6 + a_7) / C_2, \quad b_7 = -(a_6 + a_{16}) / C_2 \\ b_8 &= -(a_7 + a_{17}) / C_2, \quad b_9 = -(a_{16} + a_{17}) / C_2 \\ b_{10} &= b_7, \quad b_{11} = b_8 \end{aligned}$$

We have

$$\begin{aligned} P_2'(t) &= b_6 P_1(t) + b_7 P_2(t) + b_8 P_3(t) + b_4 P_4(t) \\ &\quad + b_{10} \text{Piep}(t) + b_{11} \text{Pied}(t) & \text{-----(18)} \end{aligned}$$

The differential equation for $P_3(t)$ is

$$\begin{aligned} C_3 P_3'(t) &= f_4(t) - f_6(t) \\ P_3'(t) &= b_{12} P_1(t) + b_{13} P_2(t) + b_{14} P_3(t) + b_{15} P_4(t) \\ &\quad + b_{16} \text{Piep}(t) + b_{17} \text{Pied}(t) & \text{-----(19)} \end{aligned}$$

The differential equation for $P_4(t)$ is

$$\begin{aligned} C_4 P_4'(t) &= f_5(t) + f_6(t) - f_8(t) \\ P_4'(t) &= b_{18} P_2(t) + b_{19} P_3(t) + b_{20} P_4(t) \\ &\quad + b_{21} \text{Piep}(t) + b_{22} \text{Pied}(t) + b_{23} P_e(t) & \text{-----(20)} \end{aligned}$$

[APPENDIX 2].

The terms involved in the performance function are expanded as

$$\begin{aligned} \alpha_1 (P_1')^2 \\ = \alpha_1 (b_0 U_0 + b_1 P_1 + b_2 P_2 + b_3 P_3 + b_4 U_i + b_5 U_n)^2 \end{aligned}$$

$$= \alpha 1 [b_0^2 U_0^2 + b_1^2 P_1^2 + b_2^2 P_2^2 + b_3^2 P_3^2 + b_4^2 U_i^2 + b_5^2 U_n^2 + 2(b_0 b_1 U_0 P_1 + b_0 b_2 U_0 P_2 + b_0 b_3 U_0 P_3 + b_0 b_4 U_0 U_i + b_0 b_5 U_0 U_n + b_1 b_2 P_1 P_2 + b_1 b_3 P_1 P_3 + b_1 b_4 P_1 U_i + b_1 b_5 P_1 U_n + b_2 b_3 P_2 P_3 + b_2 b_4 P_2 U_i + b_2 b_5 P_2 U_n + b_3 b_4 P_3 U_i + b_3 b_5 P_3 U_n + b_4 b_5 U_i U_n)]$$

$$\alpha 2 (P_2')^2 = \alpha 2 (b_9 P_4 + b_6 P_1 + b_7 P_2 + b_8 P_3 + b_{10} U_i + b_{11} U_n)^2 = \alpha 2 [b_9^2 P_4^2 + b_6^2 P_1^2 + b_7^2 P_2^2 + b_8^2 P_3^2 + b_{10}^2 U_i^2 + b_{11}^2 U_n^2 + 2(b_9 b_6 P_4 P_1 + b_9 b_7 P_4 P_2 + b_9 b_8 P_4 P_3 + b_9 b_{10} P_4 U_i + b_9 b_{11} P_4 U_n + b_6 b_7 P_1 P_2 + b_6 b_8 P_1 P_3 + b_6 b_{10} P_1 U_i + b_6 b_{11} P_1 U_n + b_7 b_8 P_2 P_3 + b_7 b_{10} P_2 U_i + b_7 b_{11} P_2 U_n + b_8 b_{10} P_3 U_i + b_8 b_{11} P_3 U_n + b_{10} b_{11} U_i U_n)]$$

$$\alpha 3 (P_3')^2 = \alpha 3 (b_{15} P_4 + b_{12} P_1 + b_{13} P_2 + b_{14} P_3 + b_{16} U_i + b_{17} U_n)^2 = \alpha 3 [b_{15}^2 P_4^2 + b_{12}^2 P_1^2 + b_{13}^2 P_2^2 + b_{14}^2 P_3^2 + b_{16}^2 U_i^2 + b_{17}^2 U_n^2 + 2(b_{15} b_{12} P_4 P_1 + b_{15} b_{13} P_4 P_2 + b_{15} b_{14} P_4 P_3 + b_{15} b_{16} P_4 U_i + b_{15} b_{17} P_4 U_n + b_{12} b_{13} P_1 P_2 + b_{12} b_{14} P_1 P_3 + b_{12} b_{16} P_1 U_i + b_{12} b_{17} P_1 U_n + b_{13} b_{14} P_2 P_3 + b_{13} b_{16} P_2 U_i + b_{13} b_{17} P_2 U_n + b_{14} b_{16} P_3 U_i + b_{14} b_{17} P_3 U_n + b_{16} b_{17} U_i U_n)]$$

$$\alpha 4 (P_4')^2 = \alpha 4 (b_{20} P_4 + b_{23} U_e + b_{18} P_2 + b_{19} P_3 + b_{21} U_i + b_{22} U_n)^2 = \alpha 4 [b_{20}^2 P_4^2 + b_{23}^2 U_e^2 + b_{18}^2 P_2^2 + b_{19}^2 P_3^2 + b_{21}^2 U_i^2 + b_{22}^2 U_n^2 + 2(b_{20} b_{23} P_4 U_e + b_{20} b_{18} P_4 P_2 + b_{20} b_{19} P_4 P_3 + b_{20} b_{21} P_4 U_i + b_{20} b_{22} P_4 U_n + b_{23} b_{18} U_e P_2 + b_{23} b_{19} U_e P_3 + b_{23} b_{21} U_e U_i + b_{23} b_{22} U_e U_n + b_{18} b_{19} P_2 P_3 + b_{18} b_{21} P_2 U_i + b_{18} b_{22} P_2 U_n + b_{19} b_{21} P_3 U_i + b_{19} b_{22} P_3 U_n + b_{21} b_{22} U_i U_n)]$$

By gathering the similar terms such that

$$U_0^2 (\alpha 1 b_0^2 + \beta 1) \\ U_i^2 (\alpha 1 b_4^2 + \alpha 2 b_{10}^2 + \alpha 3 b_{16}^2 + \alpha 4 b_{21}^2 + \beta 3) \\ U_n^2 (\alpha 1 b_5^2 + \alpha 2 b_{11}^2 + \alpha 3 b_{17}^2 + \alpha 4 b_{22}^2 + \beta 4) \\ U_e^2 (\alpha 4 b_{23}^2 + \beta 2)$$

$$P_1^2 (\alpha 1 b_1^2 + \alpha 2 b_6^2 + \alpha 3 b_{12}^2) \\ P_2^2 (\alpha 1 b_2^2 + \alpha 2 b_7^2 + \alpha 3 b_{13}^2 + \alpha 4 b_{18}^2) \\ P_3^2 (\alpha 1 b_3^2 + \alpha 2 b_8^2 + \alpha 3 b_{14}^2 + \alpha 4 b_{19}^2) \\ P_4^2 (\alpha 2 b_9^2 + \alpha 3 b_{15}^2 + \alpha 4 b_{20}^2)$$

$$2 U_0 P_1 (\alpha 1 b_0 b_1) \\ 2 U_0 P_2 (\alpha 1 b_0 b_2) + 2 U_0 P_3 (\alpha 1 b_0 b_3) \\ 2 U_0 U_i (\alpha 1 b_0 b_4) + 2 U_0 U_n (\alpha 1 b_0 b_5)$$

$$2 P_1 P_2 (\alpha 1 b_1 b_2 + \alpha 2 b_6 b_7 + \alpha 3 b_{12} b_{13}) \\ 2 P_1 P_3 (\alpha 1 b_1 b_3 + \alpha 2 b_6 b_8 + \alpha 3 b_{12} b_{14}) \\ 2 P_1 P_4 (\alpha 2 b_6 b_9 + \alpha 3 b_{12} b_{15})$$

$$2 P_2 P_3 (\alpha 1 b_2 b_3 + \alpha 2 b_7 b_8 + \alpha 3 b_{13} b_{14} + \alpha 4 b_{18} b_{19}) \\ 2 P_2 P_4 (\alpha 2 b_7 b_9 + \alpha 3 b_{13} b_{15} + \alpha 4 b_{18} b_{20}) \\ 2 P_3 P_4 (\alpha 2 b_8 b_9 + \alpha 3 b_{14} b_{15} + \alpha 4 b_{19} b_{20})$$

$$2 P_1 U_i (\alpha 1 b_1 b_4 + \alpha 2 b_6 b_{10} + \alpha 3 b_{12} b_{16}) \\ 2 P_2 U_i (\alpha 1 b_2 b_4 + \alpha 2 b_7 b_{10} + \alpha 3 b_{13} b_{16} + \alpha 4 b_{18} b_{21}) \\ 2 P_3 U_i (\alpha 1 b_3 b_4 + \alpha 2 b_8 b_{10} + \alpha 3 b_{14} b_{16} + \alpha 4 b_{19} b_{21}) \\ 2 P_4 U_i (\alpha 2 b_9 b_{10} + \alpha 3 b_{15} b_{16} + \alpha 4 b_{20} b_{21})$$

$$2 P_1 U_n (\alpha 1 b_1 b_5 + \alpha 2 b_6 b_{11} + \alpha 3 b_{12} b_{17}) \\ 2 P_2 U_n (\alpha 1 b_2 b_5 + \alpha 2 b_7 b_{11} + \alpha 3 b_{13} b_{17} + \alpha 4 b_{18} b_{22}) \\ 2 P_3 U_n (\alpha 1 b_3 b_5 + \alpha 2 b_8 b_{11} + \alpha 3 b_{14} b_{17} + \alpha 4 b_{19} b_{22}) \\ 2 P_4 U_n (\alpha 2 b_9 b_{11} + \alpha 3 b_{15} b_{17} + \alpha 4 b_{20} b_{22})$$

$$2 U_e P_2 (\alpha 4 b_{18} b_{23}) + 2 U_e P_3 (\alpha 4 b_{19} b_{23}) \\ 2 U_e P_4 (\alpha 4 b_{20} b_{23}) \\ 2 U_n U_i (\alpha 1 b_5 b_4 + \alpha 2 b_{10} b_{11} + \alpha 3 b_{16} b_{17} + \alpha 4 b_{21} b_{22}) \\ 2 U_i U_e (\alpha 4 b_{21} b_{23}) + 2 U_n U_e (\alpha 4 b_{22} b_{23})$$

Then, the Hamiltonian function is obtained as following by setting co-state variables as $q_n (n=1,2,3,4)$

$$H = d_1 U_0^2 + d_2 U_i^2 + d_3 U_n^2 + d_4 U_e^2 + d_5 P_1^2 + d_6 P_2^2 + d_7 P_3^2 + d_8 P_4^2 + d_9 U_0 P_1 + d_{10} U_0 P_2 + d_{11} U_0 P_3 + d_{12} U_0 U_i + d_{13} U_0 U_n + d_{14} P_1 P_2 + d_{15} P_1 P_3 + d_{16} P_1 P_4 + d_{17} P_2 P_3 + d_{18} P_2 P_4 + d_{19} P_3 P_4 + d_{20} P_1 U_i + d_{21} P_2 U_i + d_{22} P_3 U_i + d_{23} P_4 U_i + d_{24} P_1 U_n + d_{25} P_2 U_n + d_{26} P_3 U_n + d_{27} P_4 U_n + d_{28} P_2 U_e + d_{29} P_3 U_e + d_{30} P_4 U_e + d_{31} U_i U_n + d_{32} U_i U_e + d_{33} U_n U_e + q_1 (b_0 U_0 + b_1 P_1 + b_2 P_2 + b_3 P_3 + b_4 U_i + b_5 U_n) + q_2 (b_6 P_1 + b_7 P_2 + b_8 P_3 + b_9 P_4 + b_{10} U_i + b_{11} U_n) + q_3 (b_{12} P_1 + b_{13} P_2 + b_{14} P_3 + b_{15} P_4 + b_{16} U_i + b_{17} U_n) + q_4 (b_{18} P_2 + b_{19} P_3 + b_{20} P_4 + b_{21} U_i + b_{22} U_n + b_{23} U_e)$$

[APPENDIX 3].

The optimal control U_i, U_n, U_e and U_0 can be obtained by differentiating the Hamiltonian with respect to them.

$$\frac{\partial H}{\partial U_0} = 2 d_1 U_0 + d_9 P_1 + d_{10} P_2 + d_{11} P_3 + d_{12} U_i + d_{13} U_n + q_1 b_0 = 0$$

Then, we have

$$2 d_1 U_0 + d_{12} U_i + d_{13} U_n = G_1$$

where

$$G_1 = -d_9 P_1 - d_{10} P_2 - d_{11} P_3 - b_0 q_1$$

$$\frac{\partial H}{\partial U_i} = 2 d_2 U_i + d_{12} U_0 + d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{23} P_4 + d_{31} U_n + d_{32} U_e + b_4 q_1 + b_{10} q_2 + b_{16} q_3 + b_{21} q_4 = 0$$

Then, we have

$$d_{12} U_0 + 2 d_2 U_i + d_{31} U_n + d_{32} U_e = G_2$$

where

$$G_2 = -(d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{23} P_4 + b_4 q_1 + b_{10} q_2 + b_{16} q_3 + b_{21} q_4)$$

$$\frac{\partial H}{\partial U_n} = d_3 U_n + d_{13} U_0 + d_{24} P_1 + d_{25} P_2 + d_{26} P_3 + d_{27} P_4 + d_{31} U_i + d_{33} U_e + b_5 q_1 + b_{11} q_2 + b_{17} q_3 + b_{22} q_4 = 0$$

Then, we have

$$d_{13} U_0 + 2 d_3 U_n + d_{31} U_i + d_{33} U_e = G_3$$

where

$$G_3 = -(2 d_3 U_n + d_{24} P_1 + d_{25} P_2 + d_{26} P_3 + d_{27} P_4 + b_5 q_1 + b_{11} q_2 + b_{17} q_3 + b_{22} q_4)$$

$$\frac{\partial H}{\partial U_e} = 2 d_4 U_e + d_{28} P_2 + d_{29} P_3 + d_{30} P_4 + d_{32} U_i + d_{33} U_n + b_{23} q_4 = 0$$

Then, we have

$$d_{32} U_i + d_{33} U_n + 2 d_4 U_e = G_4$$

where

$$G_4 = -(d_{28} P_2 + d_{29} P_3 + d_{30} P_4 + b_{23} q_4)$$

Therefore we have four linear simultaneous differential equations for U_n, U_i, U_0 and U_e

$$\begin{aligned} 2 d_1 U_0 + d_{12} U_i + d_{13} U_n &= G_1 \\ d_{12} U_0 + 2 d_2 U_i + d_{31} U_n + d_{32} U_e &= G_2 \\ d_{13} U_0 + 2 d_3 U_n + d_{31} U_i + d_{33} U_e &= G_3 \\ d_{32} U_i + d_{33} U_n + 2 d_4 U_e &= G_4 \end{aligned}$$

By solving these linear algebraic equations, we have

$$\begin{aligned} U_n &= d_{55} G_1 + d_{56} G_2 + d_{57} G_3 + d_{58} G_4 \\ U_i &= d_{46} G_1 + d_{47} G_2 + d_{48} G_3 + d_{45} U_n \\ U_0 &= (G_1 - d_{12} U_i - d_{13} U_n) / (2 d_1) \\ U_e &= (G_2 - d_{12} U_0 - 2 d_2 U_i - d_{31} U_n) / d_{32} \end{aligned}$$

$$G_2 = -(d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{23} P_4 + b_4 q_1 + b_{10} q_2 + b_{16} q_3 + b_{21} q_4)$$

$$G_3 = -(d_{24} P_1 + d_{25} P_2 + d_{26} P_3 + d_{27} P_4 + b_5 q_1 + b_{11} q_2 + b_{17} q_3 + b_{22} q_4)$$

$$G_4 = -(d_{28} P_2 + d_{29} P_3 + d_{30} P_4 + b_{23} q_4)$$

U_n is thus, obtained by substituting $G_n (n=1,2,3,4)$

$$\begin{aligned} U_n &= -d_{55} (d_9 P_1 + d_{10} P_2 + d_{11} P_3 + b_0 q_1) \\ &\quad -d_{56} (d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{24} P_4 \\ &\quad + b_4 q_1 + b_{10} q_2 + b_{16} q_3 + b_{21} q_4) \\ &\quad -d_{57} (\dots + b_{22} q_4) - d_{58} (d_{28} P_2 + \dots + b_{23} q_4) \end{aligned}$$

Rearrange

$$\begin{aligned} U_n &= P_1 (-d_{55} d_9 - d_{56} d_{20} - d_{57} d_{24}) \\ &\quad + P_2 (-d_{55} d_{10} - d_{56} d_{21} - d_{57} d_{25} - d_{58} d_{28}) \\ &\quad + P_3 (-d_{55} d_{11} - d_{56} d_{22} - d_{57} d_{26} - d_{58} d_{29}) \\ &\quad + P_4 (-d_{56} d_{23} - d_{57} d_{27} - d_{58} d_{30}) \\ &\quad + q_1 (-d_{55} b_0 - d_{56} b_4 - d_{57} b_5) \\ &\quad + q_2 (-d_{56} b_{10} - d_{57} b_{11}) \\ &\quad + q_3 (-d_{56} b_{16} - d_{57} b_{17}) \\ &\quad + q_4 (-d_{56} b_{21} - d_{57} b_{22} - d_{58} b_{23}) \end{aligned}$$

Putting

$$\begin{aligned} h_1 &= -d_{55} d_9 - d_{56} d_{20} - d_{57} d_{24} \\ h_2 &= -d_{55} d_{10} - d_{56} d_{21} - d_{57} d_{25} - d_{58} d_{28} \\ h_3 &= -d_{55} d_{11} - d_{56} d_{22} - d_{57} d_{26} - d_{58} d_{29} \\ h_4 &= -d_{56} d_{23} - d_{57} d_{27} - d_{58} d_{30} \\ h_5 &= -d_{55} b_0 - d_{56} b_4 - d_{57} b_5 \\ h_6 &= -d_{56} b_{10} - d_{57} b_{11} \\ h_7 &= -d_{56} b_{16} - d_{57} b_{17} \\ h_8 &= -d_{56} b_{21} - d_{57} b_{22} - d_{58} b_{23} \end{aligned}$$

Then, we have

$$U_n = h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 + h_7 q_3 + h_8 q_4$$

$$\begin{aligned} U_i &= -d_{46} (d_9 P_1 + d_{10} P_2 + d_{11} P_3 + b_0 q_1) \\ &\quad -d_{47} (d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{23} P_4 + b_4 q_1 \\ &\quad + b_{10} q_2 + b_{16} q_3 + b_{21} q_4) \\ &\quad -d_{48} (d_{24} P_1 + d_{25} P_2 + d_{26} P_3 + 27 P_4 + b_5 q_1 \\ &\quad + b_{11} q_2 + b_{17} q_3 + b_{22} q_4) \\ &\quad -d_{45} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\ &\quad + h_7 q_3 + h_8 q_4) \end{aligned}$$

$$\begin{aligned} U_i &= P_1 (-d_{46} d_9 - d_{47} d_{20} - d_{48} d_{24} - d_{45} h_1) \\ &\quad + P_2 (-d_{46} d_{10} - d_{47} d_{21} - d_{48} d_{25} - d_{45} h_2) \\ &\quad + P_3 (-d_{46} d_{11} - d_{47} d_{22} - d_{48} d_{26} - d_{45} h_3) \\ &\quad + P_4 (-d_{47} d_{23} - d_{48} d_{27} - d_{45} h_4) \\ &\quad + q_1 (-d_{46} b_0 - d_{47} b_4 - d_{48} b_5 - d_{45} h_5) \\ &\quad + q_2 (-d_{47} b_{10} - d_{48} b_{11} - d_{45} h_6) \\ &\quad + q_3 (-d_{47} b_{16} - d_{48} b_{17} - d_{45} h_7) \\ &\quad + q_4 (-d_{47} b_{21} - d_{48} b_{22} - d_{45} h_8) \end{aligned}$$

Putting

$$\begin{aligned} h_9 &= -d_{46} d_9 - d_{47} d_{20} - d_{48} d_{24} - d_{45} h_1 \\ h_{10} &= -d_{46} d_{10} - d_{47} d_{21} - d_{48} d_{25} - d_{45} h_2 \\ h_{11} &= -d_{46} d_{11} - d_{47} d_{22} - d_{48} d_{26} - d_{45} h_3 \\ h_{12} &= -d_{47} d_{23} - d_{48} d_{27} - d_{45} h_4 \\ h_{13} &= -d_{46} b_0 - d_{47} b_4 - d_{48} b_5 - d_{45} h_5 \\ h_{14} &= -d_{47} b_{10} - d_{48} b_{11} - d_{45} h_6 \\ h_{15} &= -d_{47} b_{16} - d_{48} b_{17} - d_{45} h_7 \\ h_{16} &= -d_{47} b_{21} - d_{48} b_{22} - d_{45} h_8 \end{aligned}$$

Thus, we have

$$U_i = h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 + h_{14} q_2 + h_{15} q_3 + h_{16} q_4$$

$$\begin{aligned} U_0 &= (G_1 - d_{12} U_i - d_{13} U_n) / (2 d_1) \\ &= [-d_9 P_1 - d_{10} P_2 - d_{11} P_3 - b_0 q_1 \\ &\quad - d_{12} (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\ &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) - d_{13} (h_1 P_1 + h_2 P_2 + h_3 P_3 \\ &\quad + h_4 P_4 + h_5 q_1 + h_6 q_2 + h_7 q_3 + h_8 q_4)] / (2 d_1) \\ &= P_1 (-d_9 - d_{12} h_9 - d_{13} h_1) / (2 d_1) \\ &\quad + P_2 (-d_{10} - d_{12} h_{10} - d_{13} h_2) / (2 d_1) \\ &\quad + P_3 (-d_{11} - d_{12} h_{11} - d_{13} h_3) / (2 d_1) \\ &\quad + P_4 (-d_{12} h_{12} - d_{13} h_4) / (2 d_1) \\ &\quad + q_1 (b_0 - d_{12} h_{13} - d_{13} h_5) / (2 d_1) \\ &\quad + q_2 (-d_{12} h_{14} - d_{13} h_6) / (2 d_1) \\ &\quad + q_3 (-d_{12} h_{15} - d_{13} h_7) / (2 d_1) \\ &\quad + q_4 (-d_{12} h_{16} - d_{13} h_8) / (2 d_1) \\ &= h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\ &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4 \end{aligned}$$

$$\begin{aligned}
 U_e &= (G_2 - d_{12} U_0 - 2 d_2 U_i - d_{31} U_n) / d_{32} \\
 &= [- (d_{20} P_1 + d_{21} P_2 + d_{22} P_3 + d_{23} P_4 \\
 &\quad + b_4 q_1 + b_{10} q_2 + b_{16} q_3 + b_{21} q_4) \\
 &\quad - d_{12} (h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4) \\
 &\quad - 2 d_2 (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) \\
 &\quad - d_{31} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4)] / d_{32} \\
 &= P_1 (-d_{20} - d_{12} h_{17} - 2 d_2 h_9 - d_{31} h_1) / (d_{32}) \\
 &\quad + P_2 (-d_{21} - d_{12} h_{18} - 2 d_2 h_{10} - d_{31} h_2) / (d_{32}) \\
 &\quad + P_3 (-d_{22} - d_{12} h_{19} - 2 d_2 h_{11} - d_{31} h_3) / (d_{32}) \\
 &\quad + P_4 (-d_{23} - d_{12} h_{20} - 2 d_2 h_{12} - d_{31} h_4) / (d_{32}) \\
 &\quad + q_1 (-b_4 - d_{12} h_{21} - 2 d_2 h_{13} - d_{31} h_5) / (d_{32}) \\
 &\quad + q_2 (-b_{10} - d_{12} h_{22} - 2 d_2 h_{14} - d_{31} h_6) / (d_{32}) \\
 &\quad + q_3 (-b_{16} - d_{12} h_{23} - 2 d_2 h_{15} - d_{31} h_7) / (d_{32}) \\
 &\quad + q_4 (-b_{21} - d_{12} h_{24} - 2 d_2 h_{16} - d_{31} h_8) / (d_{32}) \\
 &= h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4
 \end{aligned}$$

[APPENDIX 4].

The optimized differential equations for the pressures are

$$\begin{aligned}
 P_1' &= b_0 U_0 + b_1 P_1 + b_2 P_2 + b_3 P_3 + b_4 U_i + b_5 U_n \\
 P_1' &= b_0 (h_{17} P_1 + h_{18} P_2 + \dots + h_{24} q_4) + b_1 P_1 + b_2 P_2 + b_3 P_3 \\
 &\quad + b_4 (h_9 P_1 + h_{10} P_2 + \dots + h_{16} q_4) + b_5 (h_1 P_1 + \dots + h_8 q_4)
 \end{aligned}$$

$$\begin{aligned}
 P_1' &= P_1 (b_0 h_{17} + b_4 h_9 + b_5 h_1 + b_1) \\
 &\quad + P_2 (b_0 h_{18} + b_4 h_{10} + b_5 h_2 + b_2) \\
 &\quad + P_3 (b_0 h_{19} + b_4 h_{11} + b_5 h_3 + b_3) \\
 &\quad + P_4 (b_0 h_{20} + b_4 h_{12} + b_5 h_4) \\
 &\quad + q_1 (b_0 h_{21} + b_4 h_{13} + b_5 h_5) \\
 &\quad + q_2 (b_0 h_{22} + b_4 h_{14} + b_5 h_6) \\
 &\quad + q_3 (b_0 h_{23} + b_4 h_{15} + b_5 h_7) \\
 &\quad + q_4 (b_0 h_{24} + b_4 h_{16} + b_5 h_8) \\
 &= J_1 P_1 + J_2 P_2 + J_3 P_3 + J_4 P_4 + J_5 q_1 + J_6 q_2 \\
 &\quad + J_7 q_3 + J_8 q_4
 \end{aligned}$$

$$\begin{aligned}
 P_2'(t) &= b_6 P_1(t) + b_7 P_2(t) + b_8 P_3(t) + b_4 P_4(t) \\
 &\quad + b_{10} U_i + b_{11} U_n \\
 &= P_1 (b_{10} h_9 + b_{11} h_1 + b_6) \\
 &\quad + P_2 (b_{10} h_{10} + b_{11} h_2 + b_7) \\
 &\quad + P_3 (b_{10} h_{11} + b_{11} h_3 + b_8) \\
 &\quad + P_4 (b_{10} h_{12} + b_{11} h_4 + b_9) \\
 &\quad + q_1 (b_{10} h_{13} + b_{11} h_5) \\
 &\quad + q_2 (b_{10} h_{14} + b_{11} h_6) \\
 &\quad + q_3 (b_{10} h_{15} + b_{11} h_7) \\
 &\quad + q_4 (b_{10} h_{16} + b_{11} h_8) \\
 &= J_9 P_1 + J_{10} P_2 + J_{11} P_3 + J_{12} P_4 + J_{13} q_1 + J_{14} q_2 \\
 &\quad + J_{15} q_3 + J_{16} q_4
 \end{aligned}$$

$$\begin{aligned}
 P_3'(t) &= b_{12} P_1(t) + b_{13} P_2(t) + b_{14} P_3(t) + b_{15} P_4(t) \\
 &\quad + b_{16} U_i + b_{17} U_n \\
 &= P_1 (b_{16} h_9 + b_{17} h_1 + b_{12}) \\
 &\quad + P_2 (b_{16} h_{10} + b_{17} h_2 + b_{13}) \\
 &\quad + P_3 (b_{16} h_{11} + b_{17} h_3 + b_{14}) \\
 &\quad + P_4 (b_{16} h_{12} + b_{17} h_4 + b_{15}) \\
 &\quad + q_1 (b_{16} h_{13} + b_{17} h_5) \\
 &\quad + q_2 (b_{16} h_{14} + b_{17} h_6) \\
 &\quad + q_3 (b_{16} h_{15} + b_{17} h_7) \\
 &\quad + q_4 (b_{16} h_{16} + b_{17} h_8) \\
 &= J_{17} P_1 + J_{18} P_2 + J_{19} P_3 + J_{20} P_4 + J_{21} q_1 \\
 &\quad + J_{22} q_2 + J_{23} q_3 + J_{24} q_4
 \end{aligned}$$

$$\begin{aligned}
 P_4'(t) &= b_{18} P_2(t) + b_{19} P_3(t) + b_{20} P_4(t) \\
 &\quad + b_{21} U_i + b_{22} U_n + b_{23} U_e \\
 &= P_1 (b_{21} h_9 + b_{22} h_1 + b_{23} h_{25}) \\
 &\quad + P_2 (b_{21} h_{10} + b_{22} h_2 + b_{23} h_{26} + b_{18}) \\
 &\quad + P_3 (b_{21} h_{11} + b_{22} h_3 + b_{23} h_{27} + b_{19}) \\
 &\quad + P_4 (b_{21} h_{12} + b_{22} h_4 + b_{23} h_{28} + b_{20}) \\
 &\quad + q_1 (b_{21} h_{13} + b_{22} h_5 + b_{23} h_{29}) \\
 &\quad + q_2 (b_{21} h_{14} + b_{22} h_6 + b_{23} h_{30}) \\
 &\quad + q_3 (b_{21} h_{15} + b_{22} h_7 + b_{23} h_{31}) \\
 &\quad + q_4 (b_{21} h_{16} + b_{22} h_8 + b_{23} h_{32}) \\
 &= J_{25} P_1 + J_{26} P_2 + J_{27} P_3 + J_{28} P_4 + J_{29} q_1 \\
 &\quad + J_{30} q_2 + J_{31} q_3 + J_{32} q_4
 \end{aligned}$$

[APPENDIX 5].

The optimized differential equations for the co-state variables.

$$q_1' = - \frac{\partial H}{\partial P_1} = - (2 d_5 P_1 + d_9 U_0 + d_{14} P_2 + d_{15} P_3 + d_{16} P_4 + d_{20} U_i + d_{24} U_n + b_1 q_1 + b_6 q_2 + b_{12} q_3)$$

Substituting the optimized control inputs

$$\begin{aligned}
 U_n &= h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4 \\
 U_i &= h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4 \\
 U_0 &= h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4 \\
 U_e &= h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4
 \end{aligned}$$

We have

$$\begin{aligned}
 &= - d_9 (h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4) \\
 &\quad - d_{20} (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) \\
 &\quad - d_{24} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4) \\
 &\quad - 2 d_5 P_1 - d_{14} P_2 - d_{15} P_3 - d_{16} P_4 \\
 &\quad - b_1 q_1 - b_6 q_2 - b_{12} q_3
 \end{aligned}$$

Rearrange

$$\begin{aligned}
 q_1' &= P_1 (-d_9 h_{17} - d_{20} h_9 - d_{24} h_1 - 2 d_5) \\
 &\quad + P_2 (-d_9 h_{18} - d_{20} h_{10} - d_{24} h_2 - d_{14}) \\
 &\quad + P_3 (-d_9 h_{19} - d_{20} h_{11} - d_{24} h_3 - d_{15}) \\
 &\quad + P_4 (-d_9 h_{20} - d_{20} h_{12} - d_{24} h_4 - d_{16}) \\
 &\quad + q_1 (-d_9 h_{21} - d_{20} h_{13} - d_{24} h_5 - b_1) \\
 &\quad + q_2 (-d_9 h_{22} - d_{20} h_{14} - d_{24} h_6 - b_6) \\
 &\quad + q_3 (-d_9 h_{23} - d_{20} h_{15} - d_{24} h_7 - b_{12}) \\
 &\quad + q_4 (-d_9 h_{24} - d_{20} h_{16} - d_{24} h_8)
 \end{aligned}$$

$$q_1' = J_{33} p_1 + J_{34} P_2 + J_{35} P_3 + J_{36} P_4 + J_{37} q_1 + J_{38} q_2 + J_{39} q_3 + J_{40} q_4$$

$$\begin{aligned}
 q_2' &= d H / d P_2 \\
 &= - (2 d_6 P_2 + d_{10} U_0 + d_{14} P_1 + d_{17} P_3 + d_{18} P_4 \\
 &\quad + d_{21} U_i + d_{25} U_n + d_{28} U_e + b_2 q_1 + b_7 q_2 \\
 &\quad + b_{13} q_3 + b_{18} q_4)
 \end{aligned}$$

Substitute the optimized control inputs

$$\begin{aligned}
 &= -d_{10} (h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4) \\
 &- d_{21} (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) \\
 &- d_{25} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4) \\
 &- d_{28} (h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4) \\
 &- (2 d_6 P_2 + d_{14} P_1 + d_{17} P_3 + d_{18} P_4 + b_2 q_1 \\
 &\quad + b_7 q_2 + b_{13} q_3 + b_{18} q_4)
 \end{aligned}$$

Rearrange

$$\begin{aligned}
 &= P_1 (-d_{10} h_{17} - d_{21} h_9 - d_{25} h_1 - d_{28} h_{25} - d_{14}) \\
 &+ P_2 (-d_{10} h_{18} - d_{21} h_{10} - d_{25} h_2 - d_{28} h_{26} - 2 d_6) \\
 &+ P_3 (-d_{10} h_{19} - d_{21} h_{11} - d_{25} h_3 - d_{28} h_{27} - d_{17}) \\
 &+ P_4 (-d_{10} h_{20} - d_{21} h_{12} - d_{25} h_4 - d_{28} h_{28} - d_{18}) \\
 &+ q_1 (-d_{10} h_{21} - d_{21} h_{13} - d_{25} h_5 - d_{28} h_{29} - b_2) \\
 &+ q_2 (-d_{10} h_{22} - d_{21} h_{14} - d_{25} h_6 - d_{28} h_{30} - b_7) \\
 &+ q_3 (-d_{10} h_{23} - d_{21} h_{15} - d_{25} h_7 - d_{28} h_{31} - b_{13}) \\
 &+ q_4 (-d_{10} h_{24} - d_{21} h_{16} - d_{25} h_8 - d_{28} h_{32} - b_{18})
 \end{aligned}$$

$$\begin{aligned}
 q_2' &= J_{41} P_1 + J_{42} P_2 + J_{43} P_3 + J_{44} P_4 \\
 &\quad + J_{45} q_1 + J_{46} q_2 + J_{47} q_3 + J_{48} q_4
 \end{aligned}$$

$$q_3' = d H / d P_3$$

$$\begin{aligned}
 &= -(2 d_7 P_3 + d_{11} U_0 + d_{15} P_1 + d_{17} P_2 + d_{19} P_4 \\
 &\quad + d_{22} U_i + d_{26} U_n + d_{29} U_e + b_3 q_1 + b_8 q_2 \\
 &\quad + b_{14} q_3 + b_{19} q_4)
 \end{aligned}$$

Substitute the optimized control inputs

$$\begin{aligned}
 &= -d_{11} (h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4) \\
 &- d_{22} (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) \\
 &- d_{26} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4) \\
 &- d_{29} (h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4) \\
 &- (2 d_7 P_3 + d_{15} P_1 + d_{17} P_2 + d_{19} P_4 + b_3 q_1 + b_8 q_2 \\
 &\quad + b_{14} q_3 + b_{19} q_4)
 \end{aligned}$$

Rearrange

$$\begin{aligned}
 &= P_1 (-d_{11} h_{17} - d_{22} h_9 - d_{26} h_1 - d_{29} h_{25} - d_{15}) \\
 &+ P_2 (-d_{11} h_{18} - d_{22} h_{10} - d_{26} h_2 - d_{29} h_{26} - d_{17}) \\
 &+ P_3 (-d_{11} h_{19} - d_{22} h_{11} - d_{26} h_3 - d_{29} h_{27} - 2 d_7) \\
 &+ P_4 (-d_{11} h_{20} - d_{22} h_{12} - d_{26} h_4 - d_{29} h_{28} - d_{19}) \\
 &+ q_1 (-d_{11} h_{21} - d_{22} h_{13} - d_{26} h_5 - d_{29} h_{29} - b_3) \\
 &+ q_2 (-d_{11} h_{22} - d_{22} h_{14} - d_{26} h_6 - d_{29} h_{30} - b_8) \\
 &+ q_3 (-d_{11} h_{23} - d_{22} h_{15} - d_{26} h_7 - d_{29} h_{31} - b_{14}) \\
 &+ q_4 (-d_{11} h_{24} - d_{22} h_{16} - d_{26} h_8 - d_{29} h_{32} - b_{19})
 \end{aligned}$$

$$\begin{aligned}
 q_3' &= J_{49} P_1 + J_{50} P_2 + J_{51} P_3 + J_{52} P_4 \\
 &\quad + J_{53} q_1 + J_{54} q_2 + J_{55} q_3 + J_{56} q_4
 \end{aligned}$$

$$q_4' = -d H / d P_4$$

$$\begin{aligned}
 &= -(2 d_8 P_4 + d_{16} P_1 + d_{18} P_2 + d_{19} P_3 \\
 &\quad + d_{23} U_i + d_{27} U_n + d_{30} U_e + b_9 q_2 + b_{15} q_3 + b_{20} q_4)
 \end{aligned}$$

Substitute the optimized control inputs

$$= -d_{23} (h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1$$

$$\begin{aligned}
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4) \\
 &- d_{27} (h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4) \\
 &- d_{30} (h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4) \\
 &- (2 d_8 P_4 + d_{16} P_1 + d_{18} P_2 + d_{19} P_3 \\
 &\quad + b_9 q_2 + b_{15} q_3 + b_{20} q_4)
 \end{aligned}$$

Rearrange

$$\begin{aligned}
 &= P_1 (-d_{23} h_9 - d_{27} h_1 - d_{30} h_{25} - d_{16}) \\
 &+ P_2 (-d_{23} h_{10} - d_{27} h_2 - d_{30} h_{26} - d_{18}) \\
 &+ P_3 (-d_{23} h_{11} - d_{27} h_3 - d_{30} h_{27} - d_{19}) \\
 &+ P_4 (-d_{23} h_{12} - d_{27} h_4 - d_{30} h_{28} - 2 d_8) \\
 &+ q_1 (-d_{23} h_{13} - d_{27} h_5 - d_{30} h_{29}) \\
 &+ q_2 (-d_{23} h_{14} - d_{27} h_6 - d_{30} h_{30} - b_9) \\
 &+ q_3 (-d_{23} h_{15} - d_{27} h_7 - d_{30} h_{31} - b_{15}) \\
 &+ q_4 (-d_{23} h_{16} - d_{27} h_8 - d_{30} h_{32} - b_{20})
 \end{aligned}$$

$$\begin{aligned}
 q_4' &= J_{57} P_1 + J_{58} P_2 + J_{59} P_3 + J_{60} P_4 \\
 &\quad + J_{61} q_1 + J_{62} q_2 + J_{63} q_3 + J_{64} q_4
 \end{aligned}$$

Associatingly, we have eight linear simultaneous optimized differential equations

$$\begin{aligned}
 P_1' &= J_1 P_1 + J_2 P_2 + J_3 P_3 + J_4 P_4 + J_5 q_1 + J_6 q_2 \\
 &\quad + J_7 q_3 + J_8 q_4
 \end{aligned}$$

$$\begin{aligned}
 P_2' &= J_9 P_1 + J_{10} P_2 + J_{11} P_3 + J_{12} P_4 + J_{13} q_1 + J_{14} q_2 \\
 &\quad + J_{15} q_3 + J_{16} q_4
 \end{aligned}$$

$$\begin{aligned}
 P_3' &= J_{17} P_1 + J_{18} P_2 + J_{19} P_3 + J_{20} P_4 + J_{21} q_1 \\
 &\quad + J_{22} q_2 + J_{23} q_3 + J_{24} q_4
 \end{aligned}$$

$$\begin{aligned}
 P_4' &= J_{25} P_1 + J_{26} P_2 + J_{27} P_3 + J_{28} P_4 + J_{29} q_1 \\
 &\quad + J_{30} q_2 + J_{31} q_3 + J_{32} q_4
 \end{aligned}$$

$$\begin{aligned}
 q_1' &= J_{33} p_1 + J_{34} P_2 + J_{35} P_3 + J_{36} P_4 \\
 &\quad + J_{37} q_1 + J_{38} q_2 + J_{39} q_3 + J_{40} q_4
 \end{aligned}$$

$$\begin{aligned}
 q_2' &= J_{41} P_1 + J_{42} P_2 + J_{43} P_3 + J_{44} P_4 \\
 &\quad + J_{45} q_1 + J_{46} q_2 + J_{47} q_3 + J_{48} q_4
 \end{aligned}$$

$$\begin{aligned}
 q_3' &= J_{49} P_1 + J_{50} P_2 + J_{51} P_3 + J_{52} P_4 \\
 &\quad + J_{53} q_1 + J_{54} q_2 + J_{55} q_3 + J_{56} q_4
 \end{aligned}$$

$$\begin{aligned}
 q_4' &= J_{57} P_1 + J_{58} P_2 + J_{59} P_3 + J_{60} P_4 \\
 &\quad + J_{61} q_1 + J_{62} q_2 + J_{63} q_3 + J_{64} q_4
 \end{aligned}$$

and four control inputs.

$$\begin{aligned}
 U_n &= h_1 P_1 + h_2 P_2 + h_3 P_3 + h_4 P_4 + h_5 q_1 + h_6 q_2 \\
 &\quad + h_7 q_3 + h_8 q_4
 \end{aligned}$$

$$\begin{aligned}
 U_i &= h_9 P_1 + h_{10} P_2 + h_{11} P_3 + h_{12} P_4 + h_{13} q_1 \\
 &\quad + h_{14} q_2 + h_{15} q_3 + h_{16} q_4
 \end{aligned}$$

$$\begin{aligned}
 U_0 &= h_{17} P_1 + h_{18} P_2 + h_{19} P_3 + h_{20} P_4 + h_{21} q_1 \\
 &\quad + h_{22} q_2 + h_{23} q_3 + h_{24} q_4
 \end{aligned}$$

$$\begin{aligned}
 U_e &= h_{25} P_1 + h_{26} P_2 + h_{27} P_3 + h_{28} P_4 + h_{29} q_1 \\
 &\quad + h_{30} q_2 + h_{31} q_3 + h_{32} q_4
 \end{aligned}$$